# Report of Preliminary Geotechnical Exploration For

Nassau WRF Improvements
Phase 1B

MAE Project No. 0110-0003D July 19, 2018

Prepared for:



Hazen and Sawyer
6675 Corporate Center Parkway, Suite 330
Jacksonville, Florida 32216



Prepared by:



8936 Western Way, Suite 12 Jacksonville, Florida 32256 Phone (904) 519-6990 Fax (904) 519-6992 July 19, 2018



Hazen and Sawyer 6675 Corporate Center Parkway, Suite 330 Jacksonville, Florida 32216

Attention: Ms. Caitlin Klug, P.E.

Reference: Report of Preliminary Geotechnical Exploration

Nassau WRF Improvements - Phase 1B

Nassau County, Florida MAE Project No. 0110-0003D

Dear Ms. Klug:

Meskel & Associates Engineering, PLLC (MAE) has completed a preliminary geotechnical exploration for the referenced project. Our work was performed in general accordance with our Subcontract Agreement for Professional Services dated June 4, 2018. The purpose of this exploration was to evaluate the subsurface conditions encountered across the project site to provide preliminary recommendations for foundation design and construction and general site preparation. A summary of our findings and recommendations are presented below; however, we recommend that this report be considered in its entirety.

As further discussed in this report, the borings generally encountered a surficial topsoil layer 4 to 7 inches thick, underlain by fine sands (SP) and fine sands with silt (SP-SM) to the boring termination depth of 20 feet below the existing ground surface. Trace to few amounts of organic fines were noted in many of the recovered samples. Groundwater was encountered at all the boring locations and measured at depths varying from 1 foot to 2 feet 7 inches below the existing ground surface. Based on our preliminary exploration, the encountered soils are suitable for support of the planned construction on conventional shallow foundation systems provided a program of site preparation is followed. The encountered soils are suitable to be reused as general site development fill across the site. However, some samples contained organic contents that would make them unsuitable for use as structural fill. In addition, the moisture content will need to be strictly controlled to achieve the required level of compaction below proposed structures. This will likely require dewatering of excavations or stockpiling of soils excavated below the groundwater level to dry before placement and compaction.

We appreciate this opportunity to be of service as your geotechnical consultant on this phase of the project. If you have any questions, or if we may be of any further service, please contact us.

Sincerely,

MESKEL & ASSOCIATES ENGINEERING, PLLC MAE FL Certificate of Authorization No. 28142

P. Rodney Mank, State of Florida, Professional Engineer, License No. 41986. This item has been electronically signed and sealed by P. Rodney Mank, P.E. on 07/19/2018 using a Digital Signature. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

W. Josh Mele, E.I.	P. Rodney Mank, P.E.	_
Staff Engineer	Principal Engineer	

Principal Engineer Licensed, Florida No. 41986

Distribution: Ms. Caitlin Klug, P.E. – Hazen and Sawyer, PC 1 pdf

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# 1.0 PROJECT INFORMATION

# 1.1 General

Project information was provided to us by Ms. Caitlin Klug, P.E., with Hazen and Sawyer, PC via several electronic correspondence and telephone conversations. We were also provided with the JEA Solicitation document No. 071-17 titled *Engineering Services for Nassau Regional Water Reclamation Facility Projects*, and several Addendum and Appendix documents associated with the comprehensive projects. In addition, we were provided with a *Wetland and Gopher Tortoise Map* prepared by Onsite Environmental Consulting, LLC, dated June 2018 for our review and reference.

# 1.2 Project Description

The site for the subject project is an undeveloped 3.5-acre parcel, located east of Art Wilson Lane and north of Radio Avenue in Nassau County, Florida. The general site location is shown on Figure 1.

Based on the provided information and our discussions with Ms. Klug, we understand that JEA will construct a remote pump station and storage tank to act as an intermediate storage and repump for the nearby Nassau Regional Water Reclamation Facility (WRF) and to accommodate peak demands for the expected growth and development of the East Nassau Community Planning Area. Detailed structural design, loading, and grading information were not available. Therefore, for the purpose of this preliminary report, we have assumed the proposed pump station equipment will be supported on a concrete slab-ongrade with a cast-in-place slab at the base of the wet well structure. Any support equipment has been assumed to also be supported on cast-in-place grade supported slabs that are relatively lightly loaded. We have assumed the proposed water storage tank will be a precast concrete tank supported on a monolithic, turned-down edge slab-on-grade. We have assumed construction areas will be supported on less than three feet of fill above the presently existing ground surface.

Our preliminary evaluations and recommendations provided in this report are based on the site information and structure assumptions as noted above. Once the final site design is complete, further geotechnical explorations should be carried out to re-evaluate site specific conditions based on final construction plans.

# 2.0 FIELD EXPLORATION

A field exploration was performed on June 15 and 16, 2018. An aerial taken from Google Earth which shows the approximate boring locations, is included as the *Boring Location Plan*, Figure 2. The boring locations were determined by us and were sent by email to you for review and approval. Once approval was granted, the GPS coordinates for each boring were obtained by overlaying the provided plan in Google Earth.

Prior to mobilizing our equipment, a Utility Locate Request was submitted to the Sunshine State One-Call Center (SSOC). Once the site utilities were located and marked, we mobilized our ATV-mounted drilling equipment. Our field personnel located each boring using a Garmin GPSMAP 78 hand-held GPS receiver; therefore, the boring locations should be considered accurate only to the degree implied by the method of layout used.



# 2.1 SPT Borings

A total of 8 Standard Penetration Test (SPT) borings were located across the site, each drilled to a depth of approximately 20 feet below the existing ground surface in general accordance with the methodology outlined in ASTM D 1586. Split-spoon soil samples recovered during performance of the borings were visually described in the field and representative portions of the samples were transported to our laboratory for classification and testing.

# 3.0 LABORATORY TESTING

Representative soil samples obtained during our field exploration were visually classified by a geotechnical engineer using the Unified Soil Classification System (USCS) in general accordance with ASTM D 2488. A Key to the Soil Classification System is included in Appendix A.

Quantitative laboratory testing was performed on selected samples of the soils encountered during the field exploration to better define the composition of the soils encountered and to provide data for correlation to their anticipated strength and compressibility characteristics. The laboratory testing determined the natural moisture content, the percent passing the U.S. No. 200 sieve (percent fines), and the organic content of the selected soil samples. The results of the laboratory testing are shown in the *Summary of Laboratory Test Results* table included in Appendix B. Also, these results are shown on the *Generalized Soil Profiles*, Figures 3 and 4, and on the *Log of Boring* records at the respective depths from which the tested samples were recovered. A description of the laboratory testing procedures is included in Appendix B.

# 4.0 GENERAL SUBSURFACE CONDITIONS

# 4.1 General Soil Profile

Graphical presentation of the generalized subsurface conditions is presented on the *Generalized Soil Profiles*, Figures 3 and 4. Detailed boring records are included in Appendix A. When reviewing the soil profiles and boring records, it should be understood that the soil conditions will vary between the boring locations. The following table summarizes the soil conditions encountered.

GENERAL SOIL PROFILE								
APPROXIMA	TE DEPTH (ft)	SOIL DESCRIPTION	USCS <sup>(1)</sup>					
FROM	то	SOIL DESCRIPTION	0303					
0	0.5	Topsoil	(2)					
0.5	8	Very loose to medium dense fine SAND and fine SAND with silt, poorly graded, occasionally with trace to few organic fines.	SP, SP-SM					
8	13	Medium dense to very dense fine SAND with silt, poorly graded, often with few amounts of organic fines.	SP-SM					
5 7		Loose to very dense fine SAND to fine SAND with silt, poorly graded.	SP, SP-SM					
(1) Unified Soil Classification System (2) Topsoil does not have an associated USCS classification								



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## 4.2 Groundwater Level

The groundwater level was encountered at each of the boring locations and recorded at the time of drilling at depths varying from 1 foot to 2 feet 7 inches below the existing ground surface. However, it should be anticipated that groundwater levels will fluctuate seasonally and with changes in climate. As such, we recommend that the water table be measured prior to construction. Measured groundwater levels are shown on the *Generalized Soil Profiles*, Figures 3 and 4, and on the soil boring logs.

# 4.3 Review of the USDA Web Soil Survey Map

The results of a review of the USDA Soil Survey Conservation Service (SSCS) Web Soil Survey of Nassau County are shown in the table below. There are two predominant soil map units at the project sight: Hurricane-Pottsburg and Mandarin fine sands. The soil drainage class, hydrological group, and estimated seasonal high groundwater levels reported in the Soil Survey are as follows:

Map Unit Symbol	Map Unit Name	Drainage Class	Hydrologic Group	Depth to the Water Table <sup>(1)</sup> (inches)
6	Hurricane-Pottsburg fine sands, 0 to 5 percent slopes	Somewhat Poorly Drained to Poorly Drained	A, A/D	12 to 42
10	Mandarin fine sand, 0 to 2 percent slopes	Somewhat Poorly Drained	А	18 to 30

<sup>&</sup>lt;sup>(1)</sup>The "Water Table" above refers to a saturated zone in the soil which occurs during specified months, typically the summer wet season. Estimates of the upper limit shown in the Web Soil Survey are based mainly on observations of the water table at selected sites and on evidence of a saturated zone, namely grayish colors (redoximorphic features) in the soil. A saturated zone that lasts for less than a month is not considered a water table.

# 4.4 Seasonal High Groundwater Level

In estimating seasonal high groundwater level, a number of factors are taken into consideration including antecedent rainfall, soil redoximorphic features (i.e., soil mottling), stratigraphy (including presence of hydraulically restrictive layers), vegetative indicators, and relief points such as drainage ditches, low-lying areas, etc.

Based on our interpretation of the current site conditions, including the boring logs and review of published data, we estimate the seasonal high groundwater levels at the site to be generally 6 to 18 inches below the ground surface at the time of our exploration. However, it should be understood that this seasonal high estimate is based on site observations and measurements at the time of our field work and on historical data on the site soil conditions. Changes in onsite stormwater drainage patterns caused by off-site development may cause seasonal high water levels to be higher or lower than historical patterns. The project drainage engineer should be consulted to evaluate the influence of these changes on groundwater levels at the site. In addition, we recommend that piezometers be installed across the site to measure groundwater fluctuations over time.

It is possible that groundwater levels may exceed the estimated seasonal high groundwater level as a result of significant or prolonged rains, which may result in ponded water in areas of the site. Therefore,



we recommend that design drawings and specifications account for the possibility of groundwater level variations, and construction planning should be based on the assumption that such variations will occur.

# 5.0 PRELIMINARY DESIGN RECOMMENDATIONS

# 5.1 General

The following preliminary evaluation and recommendations are based on the provided and assumed project information as presented in this report, and on the results of the field exploration described in this report. Once final site design is complete, we recommend a more site-specific field exploration to confirm our preliminary findings, and to develop more specific foundation and site preparation recommendations.

# 5.2 Structures

Based on the results of our field exploration, it is our opinion that the encountered subsurface conditions are adaptable to support the proposed slab-on-grade structures. The planned wet well structure can bear on the fine sands and fine sands with silt as encountered in the borings. However, very dense sands were encountered between depths of approximately 8 and 15 feet below existing grades. Therefore, difficult excavation of these sands should be expected at these depths.

We recommend an allowable net soil contact pressure of 2,000 pounds per square foot (psf) be used for shallow foundation design of the slab-on-grade structures. The wet well structure bottom slab can be designed for a net soil contact pressure of 1,000 psf. Net bearing pressure is defined as the soil bearing pressure at the foundation bearing level in excess of the natural overburden pressure at that level. The foundations should be designed based on the maximum load that could be imposed by all loading conditions.

A program of site preparation is recommended to provide a consistent soil subgrade, which will improve the load bearing capability of the subgrade soils and reduce the potential of total and differential settlements. A typical site preparation program would consist of stripping the organic topsoils within the construction area plus a 5-foot margin for each structure, then compacting the subgrade soils with vibratory equipment. Fill placed for structure support should consist of structural fill, which typically consist of fine sands and fine sands with silt. The fill should be placed in 12-inch thick loose lifts with each lift compacted to at least 95 to 98 percent of the soil's modified Proctor maximum dry density.

Small diameter tanks (i.e. tanks with diameters of 30 feet of less) and with water heights of 20 feet or less, can be supported on the existing site soils as encountered in the borings, assuming that a program of site preparation as discussed above is implemented. Larger diameter structures and structures with higher water storage heights will need additional borings within the tank structure footprint. These borings would need to continue to greater depths as their loads will impact deeper subsurface soils.

## **5.3** Borrow Considerations

Based on the subsurface soil conditions as encountered in the borings, the fine sands (SP) and fine sands with silt (SP-SM) are considered suitable for use as fill soil for general site development and as structural fill placed below proposed structures. However, it should be noted that several borings encountered soils with greater than 4 percent organic fines content. These soils are not considered suitable for use as



structural fill due to their relatively high organic content. These soils will need to stockpiled separately from other structural fill soils and can be used as embankment fill for pavements and in landscape areas. In addition, the soils containing surficial organic material (topsoil) will require removal and are also considered unsuitable for use as structural fill. They could be used in landscape berms.

It should be anticipated that soils excavated below the groundwater level at the time of construction will have moisture contents in excess of the modified Proctor optimum moisture content. Thus, the excavations will need to be dewatered prior to excavation, or the excavated soils will need to be stockpiled or spread to bring the moisture content to within 2 percent of the soil's optimum moisture content corresponding to the required degree of compaction.

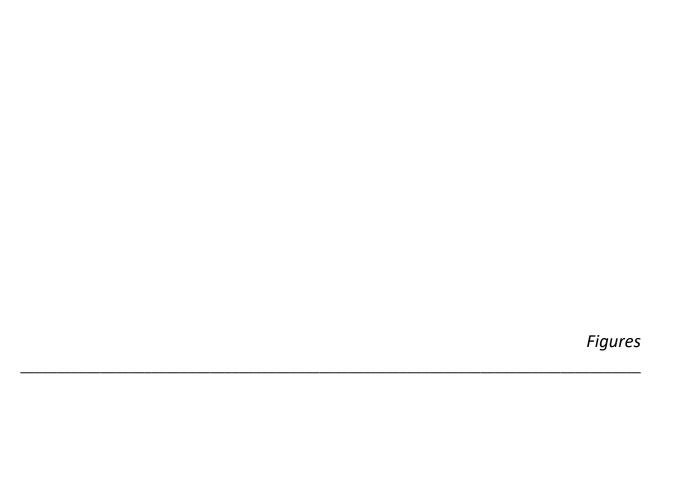
# 6.0 REPORT LIMITATIONS

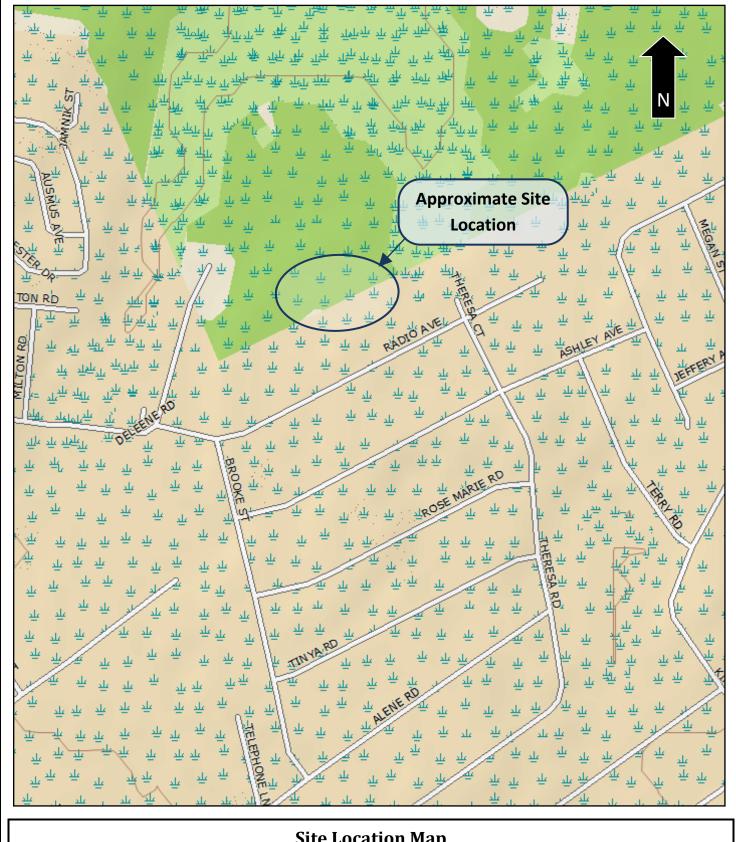
This report has been prepared for the exclusive use of Hazen and Sawyer, PC and the JEA for specific application to the design and construction of the Nassau WRF Improvements – Phase 1B project. An electronically signed and sealed version, and a version of our report that is signed and sealed in blue ink, may be considered an original of the report. Copies of an original should not be relied on unless specifically allowed by MAE in writing. Our work for this project was performed in accordance with generally accepted geotechnical engineering practice. No warranty, express or implied, is made.

The scope of our services did not include any environmental assessment or testing for the presence or absence of hazardous or toxic materials in the soil, groundwater, or surface water within or beyond the subject site. Any statements made in this report, and/or notations made on the generalized soil profiles or boring logs, regarding odors or other potential environmental concerns are based on observations made during execution of our scope of services and as such are strictly for the information of our client. No opinion of any environmental concern of such observations is made or implied. Unless complete environmental information regarding the site is already available, an environmental assessment is recommended.

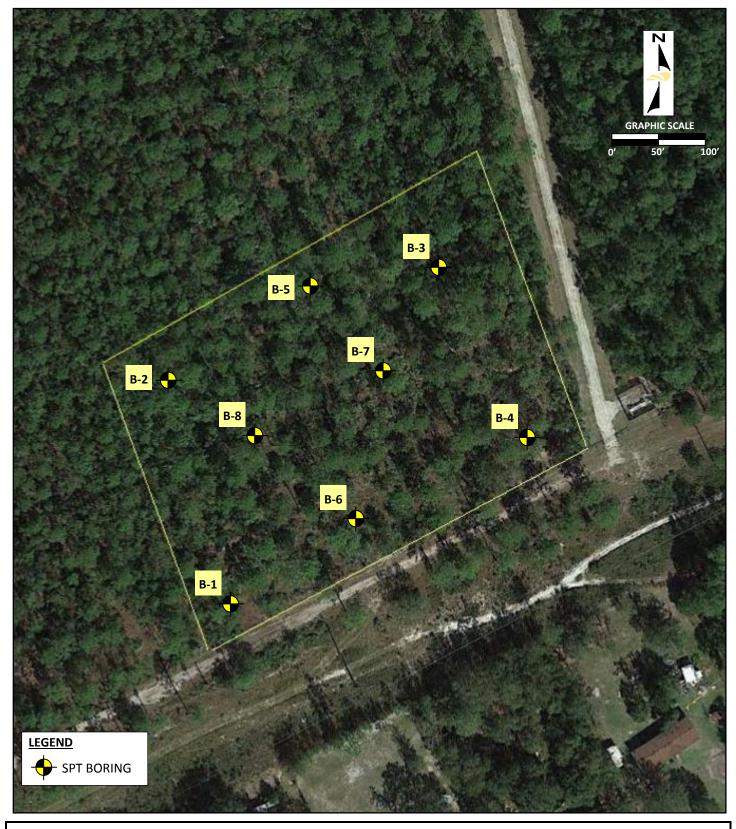
The preliminary analyses and recommendations contained in this report are based on the data obtained from the borings performed for the proposed development. This testing indicates subsurface conditions only at the specific locations and times, and only to the depths explored. These results do not reflect subsurface variations that may exist away from the boring locations and/or at depths below the boring termination depths. Subsurface conditions and water levels at other locations may differ from conditions encountered at the tested locations. In addition, it should be understood that the passage of time may result in a change in the conditions at the tested locations. Once final site design is complete, we recommend a more site-specific field exploration program to confirm our preliminary findings and recommendations. MAE is not responsible for conclusions, interpretations, opinions or recommendations made by others based on the data contained in this preliminary report.



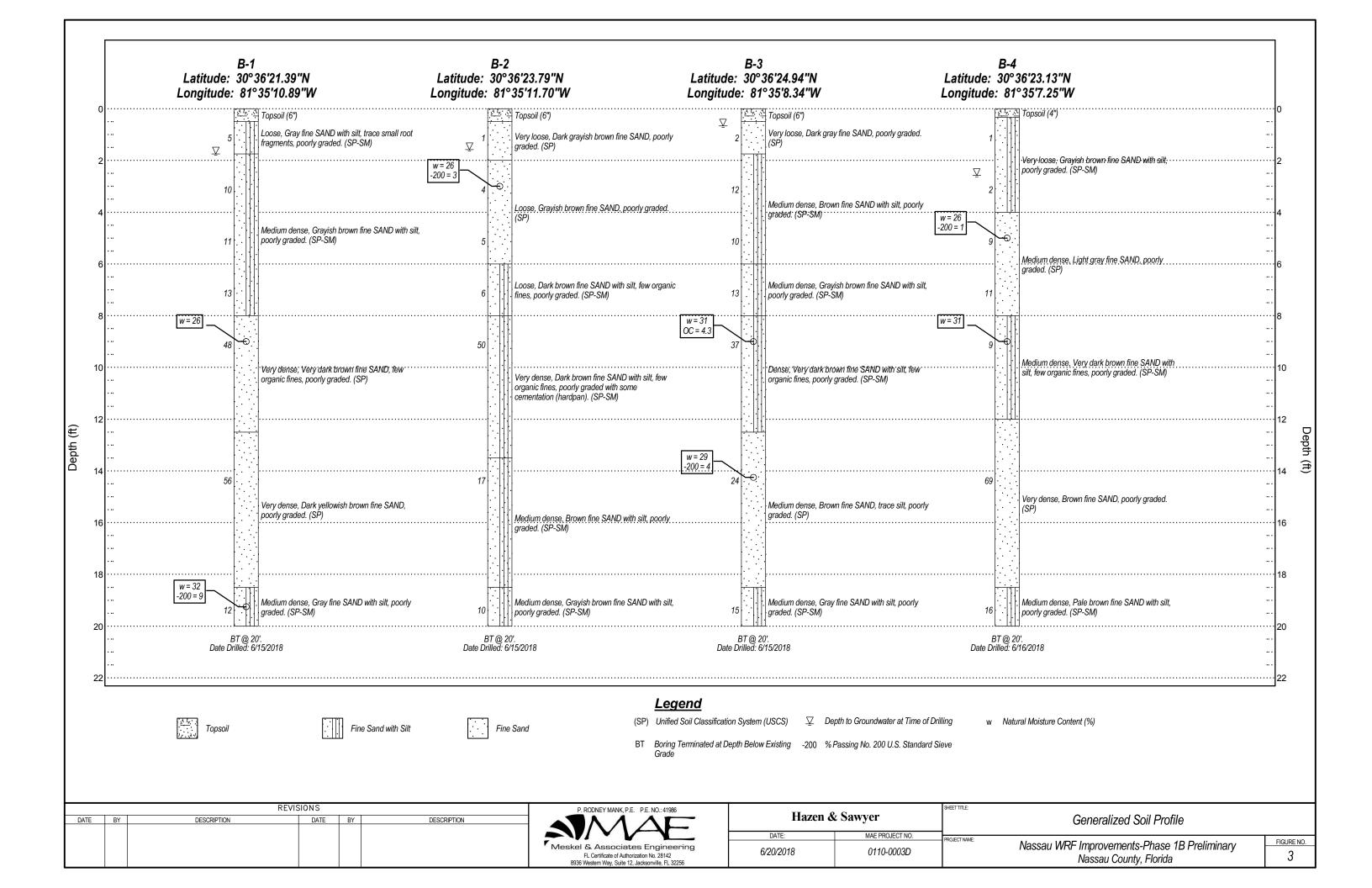


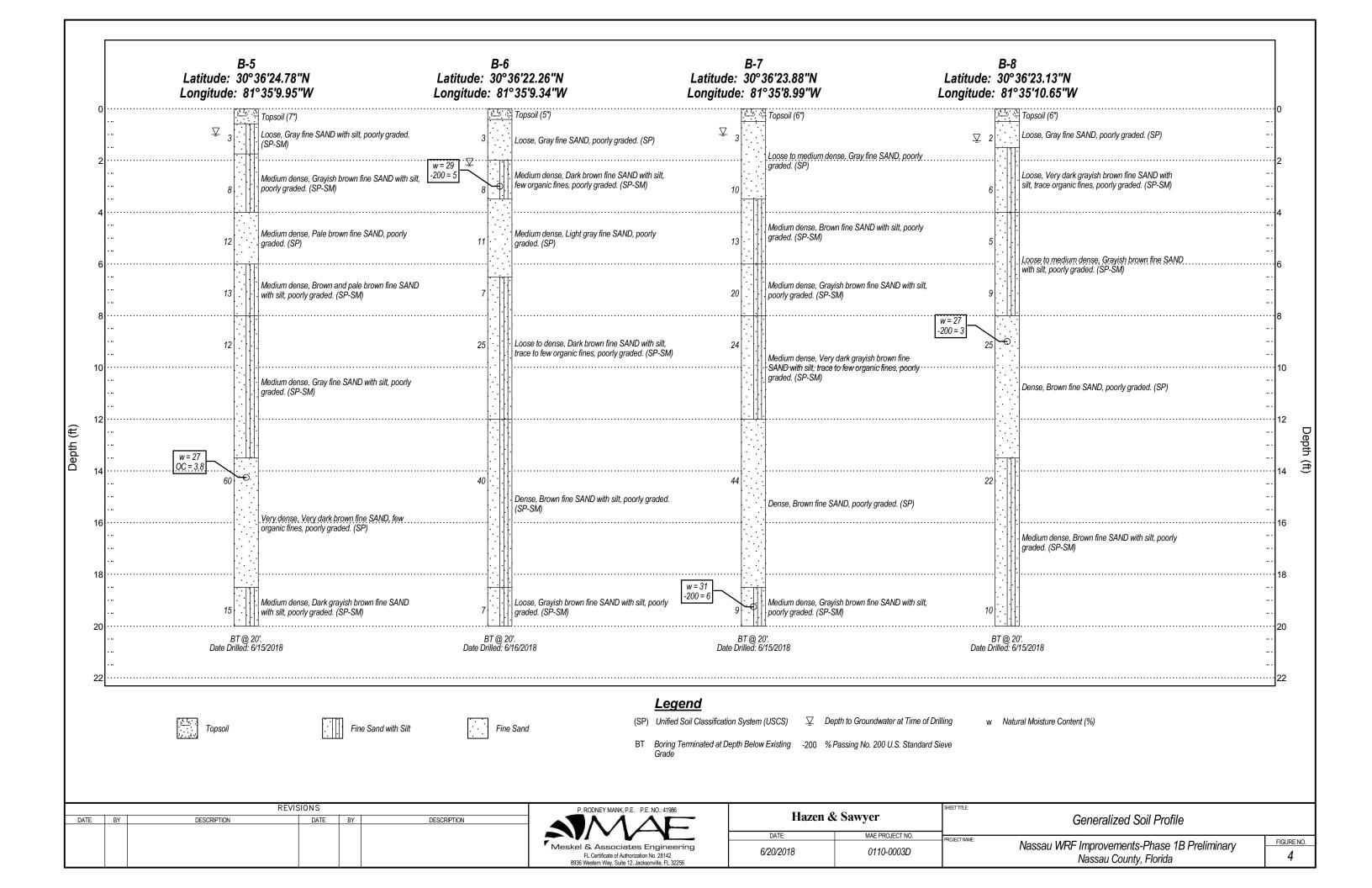


Site Location Map								
PREPARED BY PROJECT NAME								
SMAF	Nassau WRF Improvements-Pl	nase 1B Preliminary						
	Nassau County, Florida							
Meskel & Associates Engineering	REFERENCE	SCALE						
Meskel & Associates Engineering	Delorme XMap 7.0	NTS						
PREPARED FOR	MAE PROJECT NO.	FIGURE NO.						
Hazen & Sawyer	0110-0003D	1						



Boring Location Plan								
PREPARED BY PROJECT NAME								
Nassau WRF Improvements-Phas	e 1B Preliminary							
Nassau County, Florida								
REFERENCE	SCALE							
Google Earth	AS SHOWN							
MAE PROJECT NO.	FIGURE NO.							
0110-0003D	2							
	PROJECT NAME  Nassau WRF Improvements-Phas  Nassau County, Flor  REFERENCE  Google Earth  MAE PROJECT NO.							







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**BORING B-1** 

PAGE 1 OF 1 **PROJECT NO.** 0110-0003D

PRO	JJI	ECT	NAME Nassau WRF Improvements-Phase 1B Prelimin	ary						1												
PRO	PROJECT LOCATION Nassau County, Florida				CLII	ENT _	Hazer	ı & Sa	awyer													
DA	ΓΕ	STA	ARTED 6/15/18 COMPLETED 6/15/18		LAT	ITUD	E _30	)°36'2	21.39'	'N			LON	IGITU	IDE 81°35'10.89"W							
DRI	LL	ING	CONTRACTOR MAE, PLLC		DRI	LLING	MET	HOD	Sta	ndard	Pene	etratio	n Tes	st								
LO	3G	ED	BY P.R.Young CHECKED BY W. Josh	Mele	GRO	DUND	ELEV	ATIO	N _	•	_		HAN	/MER	R TYPE Automatic							
o DEPTH (ft)	SAMPLE DEPTH	NUMBER	MATERIAL DESCRIPTION	nscs	GRAPHIC LOG	BLOW COUNTS	N-VALUE	MOISTURE CONTENT (%)	CONTENT (%)	ORGANIC CONTENT (%)	LIMIT LIQUID	PLASTICITY INDEX	POCKET PEN. (tsf)	RECOVERY % (RQD)	REMARKS							
			Topsoil (6")		1   1   · · · · · · · · · · · · · · ·	1																
-	\	1	Loose, Gray fine SAND with silt, trace small root – fragments, poorly graded.	SP-SM	<b> </b> :    .	2	5															
-			<u> </u>			3																
-		2	_			2 4 6 8	10															
	(		Medium dense, Grayish brown fine SAND with silt,			2																
5	\	3	poorly graded.	SP-SM		5 6 6	11															
-			+			3																
-	٦	4	-		::   <u> </u>	6 7	13															
					<u> :   .</u>	9																
\		_				13 21	40	200														
10	\	5		SP		27 34	48	26														
10			Very dense, Very dark brown fine SAND, few organic fines, poorly graded.																			
-			-																			
-			_																			
						20																
-		6	1										20 23 33	56								
15	_					33																
-			poorly graded.	SP																		
_																						
-					· · · · ·																	
-	٦	7	Medium dense, Gray fine SAND with silt, poorly graded.	SP-SM	<b> </b> :    .	3 5 7	12	32	9													
20			Bottom of borehole at 20 feet.			7																
NO	ΓE	s _								ROU	IND V	VATE	RLE	VELS	<b>3</b>							
		_			<b>∑</b> A1	TIME	OF D	RILL	ING	1.75	ft	<u>*</u> _	ZENI	O OF	DAY							

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**BORING B-2** 

PAGE 1 OF 1 PROJECT NO. 0110-0003D

PROJECT NAME Nassau WRF Improvements-Phase 1B Preliminary PROJECT LOCATION Nassau County, Florida **CLIENT** Hazen & Sawyer DATE STARTED 6/15/18 COMPLETED 6/15/18 **LATITUDE** \_ 30°36'23.79"N **LONGITUDE** 81°35'11.70"W DRILLING CONTRACTOR MAE, PLLC **DRILLING METHOD** Standard Penetration Test **GROUND ELEVATION** LOGGED BY P.R.Young CHECKED BY W. Josh Mele HAMMER TYPE Automatic **BLOW COUNTS** PLASTICITY INDEX POCKET PEN. (tsf) SAMPLE DEPTH NUMBER MOISTURE CONTENT (%) GRAPHIC LOG ORGANIC CONTENT (% LIQUID LIMIT DEPTH (ft) N-VALUE RECOVERY (RQD) FINES CONTENT ( USCS MATERIAL DESCRIPTION **REMARKS** Topsoil (6") 0 Very loose, Dark grayish brown fine SAND, poorly 1 SP  $\nabla$ graded. 2 3 2 4 26 3 Loose, Grayish brown fine SAND, poorly graded. SP 2 2 3 5 3 Loose, Dark brown fine SAND with silt, few organic\_ 3 SP-SM 6 fines, poorly graded. 5 20 5 50 50 0 Very dense, Dark brown fine SAND with silt, few organic fines, poorly graded with some cementation | SP-SM (hardpan). 6 17 10 15 Medium dense, Brown fine SAND with silt, poorly SP-SM graded. Medium dense, Grayish brown fine SAND with silt, SP-SM 5 10 poorly graded. Bottom of borehole at 20 feet. **GROUND WATER LEVELS** NOTES  $\nabla$  AT TIME OF DRILLING 1.58 ft  $^*$ ablaEND OF DAY $\_{---}$ 

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**BORING B-3** 

PAGE 1 OF 1 PROJECT NO. 0110-0003D

PROJECT NAME Nassau WRF Improvements-Phase 1B Preliminary PROJECT LOCATION Nassau County, Florida **CLIENT** Hazen & Sawyer DATE STARTED 6/15/18 **COMPLETED** \_6/15/18 **LATITUDE** 30°36'24.94"N **LONGITUDE** 81°35'8.34"W DRILLING CONTRACTOR MAE, PLLC **DRILLING METHOD** Standard Penetration Test **GROUND ELEVATION** LOGGED BY P.R.Young CHECKED BY W. Josh Mele HAMMER TYPE Automatic **BLOW COUNTS** PLASTICITY INDEX POCKET PEN. (tsf) MOISTURE CONTENT (%) SAMPLE DEPT NUMBER GRAPHIC LOG ORGANIC CONTENT (% LIQUID LIMIT DEPTH (ft) N-VALUE RECOVERY (RQD) FINES CONTENT ( **USCS** MATERIAL DESCRIPTION **REMARKS** Topsoil (6") 0 2 2 2 Very loose, Dark gray fine SAND, poorly graded. SP 3 2 12 8 9 Medium dense, Brown fine SAND with silt, poorly SP-SM 3 5 5 3 10 8 Medium dense, Grayish brown fine SAND with silt, 6 SP-SM 13 poorly graded. 8 5 5 37 31 4.3 26 28 Dense, Very dark brown fine SAND with silt, few SP-SM organic fines, poorly graded. 6 29 24 4 13 15 Medium dense, Brown fine SAND, trace silt, poorly SP graded. Medium dense, Gray fine SAND with silt, poorly SP-SM 6 15 graded. Bottom of borehole at 20 feet. **GROUND WATER LEVELS** NOTES  $\nabla$  AT TIME OF DRILLING 0.67 ft  $^*$ ablaEND OF DAY $\_{---}$ 

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**BORING B-4** 

PAGE 1 OF 1 PROJECT NO. 0110-0003D

PROJECT NAME Nassau WRF Improvements-Phase 1B Preliminary PROJECT LOCATION Nassau County, Florida **CLIENT** Hazen & Sawyer DATE STARTED 6/16/18 COMPLETED 6/16/18 **LATITUDE** \_ 30°36'23.13"N **LONGITUDE** 81°35'7.25"W DRILLING CONTRACTOR MAE, PLLC **DRILLING METHOD** Standard Penetration Test **GROUND ELEVATION** LOGGED BY P.R.Young CHECKED BY W. Josh Mele HAMMER TYPE Automatic SAMPLE DEPTH NUMBER **BLOW COUNTS** PLASTICITY INDEX POCKET PEN. (tsf) MOISTURE CONTENT (%) GRAPHIC LOG ORGANIC CONTENT (% LIQUID LIMIT DEPTH (ft) N-VALUE RECOVERY (RQD) FINES CONTENT ( **USCS** MATERIAL DESCRIPTION **REMARKS** Topsoil (4") 0 1 0 Very loose, Grayish brown fine SAND with silt, SP-SM 0 2 2 2 3 9 26 5 Medium dense, Light gray fine SAND, poorly SP 6 11 5 5 3 5 9 31 6 Medium dense, Very dark brown fine SAND with SP-SM silt, few organic fines, poorly graded. 6 40 69 29 15 SP Very dense, Brown fine SAND, poorly graded. Medium dense, Pale brown fine SAND with silt, SP-SM 8 16 poorly graded. Bottom of borehole at 20 feet. **GROUND WATER LEVELS NOTES**  $\nabla$  AT TIME OF DRILLING 2.58 ft  $^*$ ablaEND OF DAY $\_{---}$ 

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**BORING B-5** 

PAGE 1 OF 1 PROJECT NO. 0110-0003D

PROJECT NAME Nassau WRF Improvements-Phase 1B Preliminary PROJECT LOCATION Nassau County, Florida **CLIENT** Hazen & Sawyer DATE STARTED 6/15/18 COMPLETED 6/15/18 **LATITUDE** \_ 30°36'24.78"N **LONGITUDE** 81°35'9.95"W DRILLING CONTRACTOR MAE, PLLC **DRILLING METHOD** Standard Penetration Test **GROUND ELEVATION** LOGGED BY P.R.Young CHECKED BY W. Josh Mele HAMMER TYPE Automatic SAMPLE DEPTH NUMBER **BLOW COUNTS** PLASTICITY INDEX POCKET PEN. (tsf) MOISTURE CONTENT (%) GRAPHIC LOG ORGANIC CONTENT (% LIQUID LIMIT DEPTH (ft) N-VALUE RECOVERY (RQD) FINES CONTENT ( **USCS** MATERIAL DESCRIPTION **REMARKS** 0 Topsoil (7") 3 Loose, Gray fine SAND with silt, poorly graded. SP-SM 2 2 Medium dense, Grayish brown fine SAND with silt, 4 SP-SM 2 8 poorly graded. 8 8 Medium dense, Pale brown fine SAND, poorly 5 3 SP 12 graded. 8 Medium dense, Brown and pale brown fine SAND 6 SP-SM 4 13 with silt, poorly graded. 9 6 5 12 6 Medium dense, Gray fine SAND with silt, poorly SP-SM graded. 22 6 29 27 60 3.8 15 Very dense, Very dark brown fine SAND, few SP organic fines, poorly graded. Medium dense, Dark grayish brown fine SAND SP-SM 15 with silt, poorly graded. 8 Bottom of borehole at 20 feet. **GROUND WATER LEVELS** NOTES  $\nabla$  AT TIME OF DRILLING 1.00 ft  $^*$ ablaEND OF DAY $\_{---}$ 

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NEW MAE LOG LAT/LONG-EOD-HA - NEW TEMPLATE 7-30-12.GDT - 7/19/18 13:58 - F./GINT/GINT FILES/PROJECTS/0/10-0003D/PHASE 1B-PRELIMINARY.GPJ



**BORING B-6** 

PAGE 1 OF 1 **PROJECT NO.** 0110-0003D

	PROJECT NAME Nassau WRF Improvements-Phase 1B Preliminary  PROJECT LOCATION Nassau County, Florida  CLIENT Hazen & Sawyer														
			LOCATION   Nassau County, Florida				Hazer E _30						1.00	ICITI IDE	31°35'9.34"W
			CONTRACTOR MAE, PLLC				MET				Pene	etratio			31 33 9.34 W
			BY P.R.Young CHECKED BY W. Josh N	Mele			ELEV							MER TYPE	Au <del>to</del> matic
								ĺ							
o DEPTH (ft)	SAMPLE DEPTI	NUMBER	MATERIAL DESCRIPTION	nscs	GRAPHIC LOG	BLOW COUNTS	N-VALUE	MOISTURE CONTENT (%)	FINES CONTENT (%)	ORGANIC CONTENT (%)	LIQUID	PLASTICITY INDEX	POCKET PEN. (tsf)	RECOVERY % (RQD)	REMARKS
- \	\	1	Topsoil (5")  Loose, Gray fine SAND, poorly graded.	SP	7,1 1.7.7.7	1 1 2	3								
-	\	2	Medium dense, Dark brown fine SAND with silt, few organic fines, poorly graded.	SP-SM		2 2 3	8	29	5						
		_				5 6		20							
5		3	Medium dense, Light gray fine SAND, poorly graded.	SP		3 5 6 6	11								
-			1			3	_								
-		4				3	7								
10		5	Loose to dense, Dark brown fine SAND with silt, trace to few organic fines, poorly graded.	SP-SM		4 10 15 18	25								
-			-												
- -	1	6				15 22 18	40								
_15			Dense, Brown fine SAND with silt, poorly graded. SP-S	SP-SM		10									
- -			_												
20		7	graded.	SP-SM		2 3 4	7								
			Bottom of borehole at 20 feet.												
							ļ								
NO.	ΓΕ	s _												VELS	
		_			abla AT	TIME	OF D	RILL	ING_	2.17	ft	* <u>\</u>	ZEND	OF DAY	<del></del>

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MAE LOG LAT/LONG-EOD-HA - NEW TEMPLATE 7-30-12.GDT - 7/19/18 13:58 - F.\GINT\GINT FILES\PROJECTS\0110-0003D\PHASE 1B-PRELIMINARY.GPJ

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**BORING B-7** 

PAGE 1 OF 1 PROJECT NO. 0110-0003D

**PROJECT NAME** Nassau WRF Improvements-Phase 1B Preliminary PROJECT LOCATION Nassau County, Florida **CLIENT** Hazen & Sawyer DATE STARTED 6/15/18 COMPLETED 6/15/18 **LATITUDE** 30°36'23.88"N **LONGITUDE** 81°35'8.99"W DRILLING CONTRACTOR MAE, PLLC **DRILLING METHOD** Standard Penetration Test CHECKED BY W. Josh Mele **GROUND ELEVATION** LOGGED BY P.R.Young HAMMER TYPE Automatic SAMPLE DEPTH NUMBER **BLOW COUNTS** PLASTICITY INDEX POCKET PEN. (tsf) MOISTURE CONTENT (%) GRAPHIC LOG ORGANIC CONTENT (% LIQUID LIMIT DEPTH (ft) N-VALUE RECOVERY (RQD) FINES CONTENT ( **USCS** MATERIAL DESCRIPTION **REMARKS** Topsoil (6")  $\nabla$ 3 2 Loose to medium dense, Gray fine SAND, poorly SP graded. 2 2 10 6 7 3 Medium dense, Brown fine SAND with silt, poorly SP-SM 5 8 3 graded. 13 10 Medium dense, Grayish brown fine SAND with silt, 9 SP-SM 4 20 poorly graded. 11 5 24 15 Medium dense, Very dark grayish brown fine 21 SAND with silt, trace to few organic fines, poorly SP-SM graded. 6 21 44 23 15 SP Dense, Brown fine SAND, poorly graded. Medium dense, Grayish brown fine SAND with silt, SP-SM 3 9 31 6 poorly graded. Bottom of borehole at 20 feet. **GROUND WATER LEVELS** NOTES  $\nabla$  AT TIME OF DRILLING 1.00 ft  $^*$ ablaEND OF DAY $\_{---}$ 

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MAE LOG LAT/LONG-EOD-HA - NEW TEMPLATE 7-30-12.GDT - 7/19/18 13:58 - F\\GINT\GINT\FILES\PROJECTS\0110-0003D\PHASE 1B-PRELIMINARY\GP\

NEW P



**BORING B-8** 

PAGE 1 OF 1 PROJECT NO. 0110-0003D

**PROJECT NAME** Nassau WRF Improvements-Phase 1B Preliminary PROJECT LOCATION Nassau County, Florida **CLIENT** Hazen & Sawyer COMPLETED 6/15/18 DATE STARTED 6/15/18 **LATITUDE** 30°36'23.13"N **LONGITUDE** 81°35'10.65"W DRILLING CONTRACTOR MAE, PLLC **DRILLING METHOD** Standard Penetration Test **GROUND ELEVATION** LOGGED BY P.R.Young CHECKED BY W. Josh Mele HAMMER TYPE Automatic SAMPLE DEPTH NUMBER **BLOW COUNTS** PLASTICITY INDEX POCKET PEN. (tsf) MOISTURE CONTENT (%) FINES CONTENT (%) GRAPHIC LOG ORGANIC CONTENT (% LIQUID LIMIT DEPTH (ft) N-VALUE RECOVERY (RQD) **USCS** MATERIAL DESCRIPTION **REMARKS** Topsoil (6") 0 2 2 SP 2 2 Loose, Very dark grayish brown fine SAND with silt, trace organic fines, poorly graded. SP-SM 2 6 6 2 2 5 3 Loose to medium dense, Grayish brown fine SAND\_ SP-SM with silt, poorly graded. 2 4 5 9 6 10 5 25 27 3 15 Dense, Brown fine SAND, poorly graded. SP 6 10 22 12 15 Medium dense, Brown fine SAND with silt, poorly SP-SM graded. 5 10 Bottom of borehole at 20 feet. **GROUND WATER LEVELS NOTES**  $\nabla$  AT TIME OF DRILLING 1.25 ft  $^*$ ablaEND OF DAY $\_{---}$ 

# FIELD EXPLORATION PROCEDURES

# **Standard Penetration Test (SPT) Borings**

The Standard Penetration Test (SPT) boring(s) were performed in general accordance with the latest revision of ASTM D 1586, "Standard Test Method for Standard Penetration Test (SPT) and Split-Barrel Sampling of Soils." The borings were advanced by rotary drilling techniques. A split-barrel sampler was inserted to the borehole bottom and driven 18 to 24 inches into the soil using a 140-pound hammer falling an average of 30 inches per hammer blow. The number of hammer blows for the final 12 inches of penetration (18" sample) or for the sum of the middle 12 inches of penetration (24" sample) is termed the "penetration resistance, blow count, or N-value." This value is an index to several in-situ geotechnical properties of the material tested, such as relative density and Young's Modulus.

After driving the sampler, it was retrieved from the borehole and representative samples of the material within the split-barrel were containerized and sealed. After completing the drilling operations, the samples for each boring were transported to the laboratory where they were examined by a geotechnical engineer to verify the field descriptions and classify the soil, and to select samples for laboratory testing.



# **KEY TO BORING LOGS - USCS**

# Soil Classification

Soil classification of samples obtained at the boring locations is based on the Unified Soil Classification System (USCS). Coarse grained soils have more than 50% of their dry weight retained on a #200 sieve. Their principal descriptors are: sand, cobbles and boulders. Fine grained soils have less than 50% of their dry weight retained on a #200 sieve. They are principally described as clays if they are plastic and silts if they are slightly to non-plastic. Major constituents may be added as modifiers and minor constituents may be added according to the relative proportions based on grain size. In addition to gradation, coarse-grained soils are defined on the basis of their in-place relative density and fine-grained soils on the basis of their consistency.

BORING LOG LEGEND							
Symbol	Description						
N	Standard Penetration Resistance, the number of blows required to advance a standard spoon sampler 12" when driven by a 140-lb hammer dropping 30".						
WOR	Split Spoon sampler advanced under the weight of the drill rods						
WOH	Split Spoon sampler advanced under the weight of the SPT hammer						
50/2"	Indicates 50 hammer blows drove the split spoon 2 inches; 50 Hammer blows for less than 6-inches of split spoon driving is considered "Refusal".						
(SP)	Unified Soil Classification System						
-200	Fines content, % Passing No. 200 U.S. Standard Sieve						
w	Natural Moisture Content (%)						
OC	Organic Content (%)						
LL	Liquid Limit						
PI	Plasticity Index						
NP	Non-Plastic						
PP	Pocket Penetrometer in tons per square foot (tsf)						

MODIFIERS							
SECONDARY CONSTITUENTS							
(Sand, Silt or Clay)							
Trace	Less than 5%						
With	5% to 12%						
Sandy, Silty or Clayey	12% to 35%						
Very Sandy, Very Silty or Very Clayey	35% to 50%						
ORGANIC CONTE	NT						
Trace	2% or less						
Few	3% to 5%						
Little	5% to 10%						
With	Greater than 10%						
AUNOR COMPONE	NITC						
MINOR COMPONE							
(Shell, Rock, Debris, Roc	ots, etc.)						
Trace	Less than 5%						
Few	5% to 10%						
Little	15% to 25%						
Some	30% to 45%						

RELATIVE DENSITY (Coarse-Grained Soils)							
Relative Density	N-Value						
Very Loose	Less than 4						
Loose	4 to 10						
Medium Dense	10 to 30						
Dense	30 to 50						
Very Dense	Greater than 50						
CONSISTENCY (Fine	CONSISTENCY (Fine-Grained Soils)						
Consistency	N-Value						
Very Soft	Less than 2						
Soft	2 to 4						
Firm	4 to 8						
Stiff	8 to 15						
Very Stiff	15 to 30						
Hard	Greater than 30						
RELATIVE HARDNE	SS (Limestone)						
Relative Hardness	N-Value						
Soft	Less than 50						
Hard	Greater than 50						



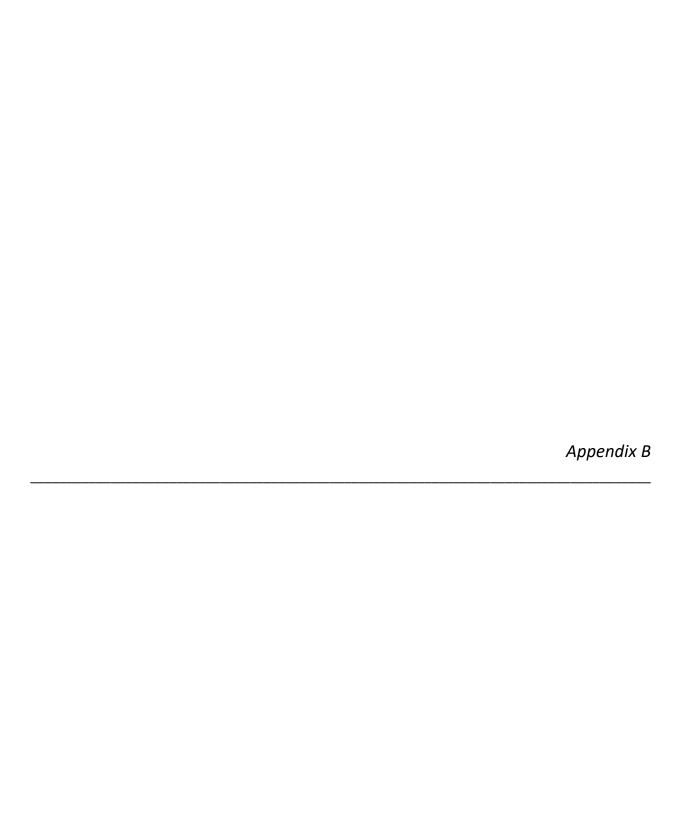
# Unified Soil Classification System (USCS) (from ASTM D 2487)

Мајс	or Divisions		Group Symbol	Typical Names		
	Gravels	Clean	GW	Well-graded gravels and gravel-sand mixtures, little or no fines		
	50% or more of coarse fraction	Gravels	GP	Poorly graded gravels and gravel-sand mixtures, little or no fines		
Coarse-Grained Soils	retained on the 4.75 mm	Gravels	GM	Silty gravels, gravel-sand-silt mixtures		
More than 50%	(No. 4) sieve	with Fines	GC	Clayey gravels, gravel-sand-clay mixtures		
retained on the 0.075 mm	Sands	Clean	SW	Well-graded sands and gravelly sands, little or no fines		
(No. 200) sieve	50% or more of coarse fraction passes the 4.75	Sands	SP	Poorly graded sands and gravelly sands, little or no fines		
		Sands	SM	Silty sands, sand-silt mixtures		
	(No. 4) sieve	with Fines	SC	Clayey sands, sand-clay mixtures		
			ML	Inorganic silts, very fine sands, rock four, silty or clayey fine sands		
	Silts and Clays Liquid Limit 50% or	less	CL	Inorganic clays of low to medium plasticity, gravelly/sandy/silty/lean clays		
Fine-Grained Soils More than 50% passes			OL	Organic silts and organic silty clays of low plasticity		
the 0.075 mm (No. 200) sieve	Silts and Clays		МН	Inorganic silts, micaceous or diatomaceous fine sands or silts, elastic silts		
	Liquid Limit greater	than 50%	СН	Inorganic clays or high plasticity, fat clays		
			ОН	Organic clays of medium to high plasticity		
Highly Organic Soils			PT	Peat, muck, and other highly organic soils		

Prefix: G = Gravel, S = Sand, M = Silt, C = Clay, O = Organic

Suffix: W = Well Graded, P = Poorly Graded, M = Silty, L = Clay, LL < 50%, H = Clay, LL > 50%





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# **SUMMARY OF LABORATORY TEST RESULTS**

**PROJECT NO.** <u>0110-0003D</u>

PROJECT NAME Nassau WRF Improvements-Phase 1B Preliminary

**DATE**. 6/25/2018

PROJECT LOCATION Nassau County, Florida				CLIENT Hazen & Sawyer						
Borehole	Sample No.	Approx. Depth (ft)	%<#200 Sieve	Water Content (%)	Organic Content (%)	Liquid Limit	Plastic Limit	Plasticity Index	USCS Classification	Comments
B-1	5	9		26					SP	
B-1	7	19	9	32					SP-SM	
B-2	2	3	3	26					SP	
B-3	9	9		31	4.3			-	SP-SM	
B-3	14	14	4	29					SP	
B-4	3	5	1	26					SP	
B-4	5	9		31					SP-SM	
B-5	6	14		27	3.8				SP	
B-6	2	3	5	29					SP-SM	
B-7	7	19	6	31					SP-SM	
B-8	5	9	3	27				-	SP	

Note: "---" Untested Parameter

# **LABORATORY TEST PROCEDURES**

# **Percent Fines Content**

The percent fines or material passing the No. 200 mesh sieve of the sample tested was determined in general accordance with the latest revision of ASTM D 1140. The percent fines are the soil particles in the silt and clay size range.

# **Natural Moisture Content**

The water content of the tested sample was determined in general accordance with the latest revision of ASTM D 2216. The water content is defined as the ratio of "pore" or "free" water in a given mass of material to the mass of solid material particles.

# **Organic Loss on Ignition (Percent Organics)**

The organic loss on ignition or percent organic material in the sample tested was determined in general accordance with ASTM D 2974. The percent organics is the material, expressed as a percentage, which is burned off in a muffle furnace at 455±10 degrees Celsius.

