



ECS Florida, LLC

Geotechnical Engineering Report

JEA Galvanized Pipe (Packages D-M)

College Street
Jacksonville, Florida

ECS Project Number 35:30388

June 4, 2020



ECS FLORIDA, LLC

"Setting the Standard for Service"

Geotechnical • Construction Materials • Environmental • Facilities

June 4, 2020

Mr. Robert Kermitz
ETM, Inc.
14775 Old St. Augustine Road
Jacksonville, Florida 32258

ECS Project No. 35:30388
Client ID: 0120

Reference: Geotechnical Engineering Report
JE A Galvanized Pipe (Packages D-M)
College Street
Jacksonville, Florida

Dear Mr. Kermitz:

ECS Florida, LLC. (ECS) has completed the subsurface exploration, laboratory testing, and geotechnical engineering analyses for the above-referenced project. Our services were performed in general accordance with the Technical Consulting Services Agreement No. 1, dated May 12, 2020. This report presents our understanding of the geotechnical aspects of the project, the results of the field exploration and laboratory testing conducted, and our design and construction recommendations.

It has been our pleasure to be of service to ETM, Inc. during the design phase of this project. We would appreciate the opportunity to remain involved during the continuation of the design phase, and we would like to provide our services during construction phase operations as well to verify the assumptions of subsurface conditions made for this report. Should you have any questions concerning the information contained in this report, or if we can be of further assistance to you, please contact us.

Respectfully submitted,

ECS Florida, LLC.

Chris M. Egan, P.E.

Geotechnical Department Manager

Registered, Florida No. 79645

CEgan@ecslimited.com

David W. Spangler, P.E.

Principal Engineer

Registered Florida No. 58770

DSpankler@ecslimited.com

Distribution: Mr. Robert Kermitz – ETM, Inc.

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- Figure 2 Roadway Soil Survey Sheet
- Figure 3 Field Exploration Plan
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- Field Exploration Procedures
- Key to Soil Classification

Appendix B – Laboratory Testing

- Laboratory Testing Summary
- Particle Size Distribution Reports
- Laboratory Test Procedures

EXECUTIVE SUMMARY

The following summarizes the main findings of the exploration, particularly those that may have a cost impact on the planned development. Further, our principal foundation recommendations are summarized. Information gleaned from the executive summary should not be utilized in lieu of reading the entire geotechnical report.

- The borings generally encountered between 2 inches and 1.1 feet of asphalt and limerock underlain by fine sand (A-3) and silty fine sand (A-2-4) to depths between 1.5 feet and 8 feet below ground surface and layers of fine sand (A-3), silty fine sand (A-2-4), clayey fine sand (A-2-6), very clayey fine sand (A-6), and clay with varying amounts of sand (A-7-6) to the boring termination depths of 10 feet below top of asphalt. Groundwater was encountered between depths of approximately 3 feet and 8.8 feet below ground surface.
- In general, we consider the subsurface conditions at the site capable of supporting the proposed pipelines when constructed on properly prepared subgrade soils. Clayey soils (A-2-6, A-6, and A-7-6) may be encountered at the pipeline invert elevations and will be required to be over-excavated and replaced as discussed in this report.
- Backfill should be placed in accordance with Section 103 of the *City Standard Specifications for City of Jacksonville Florida*.

1.0 INTRODUCTION

1.1 GENERAL

The purpose of this study was to provide geotechnical information for the design of new water pipelines in the College Street area of Jacksonville. The overall project will include understand approximately 37,000 linear feet of 2 inch, 4, inch 6 inch, and 8 inch diameter water main pipes. This report includes only the portions of the pipelines along portions of Nolan Street, Hunt Street, Edison Avenue, Lenox Avenue, Gilmore Street, Ernest Street, Dellwood Street, Myra Street, Green Street, Plum Street, College Street, College Place, Luray Street, Jasmine Place, Melba Street, Soltice Street, Owen Avenue, Willowbranch Avenue, and Rubel Street referenced as Packages D-M.

The recommendations developed for this report are based on project information supplied by ETM, Inc. This report contains the results of our subsurface explorations and laboratory testing programs, site characterization, engineering analyses, and recommendations for the design and construction of planned pipelines.

1.2 SCOPE OF SERVICES

To obtain the necessary geotechnical information required for design of proposed pipelines, 43 soil test borings were performed at locations selected by ETM, Inc. A laboratory-testing program was also implemented to characterize the physical and engineering properties of the subsurface soils.

This report discusses our exploratory and testing procedures, presents our findings and evaluations and includes the following.

- A brief review and description of our field and laboratory test procedures and the results of testing conducted.
- A review of surface topographical features and site conditions.
- A review of area and site geologic conditions.
- A review of subsurface soil stratigraphy with pertinent available physical properties.
- Final copies of our soil boring logs.
- Recommendations for site preparation and construction of compacted fills.
- Recommendations for design of the pipelines.

1.3 AUTHORIZATION

Our services were provided in accordance with the Technical Consulting Services Agreement No. 1 dated May 12, 2020 and includes the Terms and Conditions of Service outlined with the Agreement.

2.0 PROJECT INFORMATION

2.1 PROJECT LOCATION

The project site is located along portions of Nolan Street, Hunt Street, Edison Avenue, Lenox Avenue, Lenox Square, Gilmore Street, Ernest Street, Dellwood Street, Myra Street, Green Street, Plum Street, College Street, College Place, Luray Street, Jasmine Place, Melba Street, Soltice Street, Owen Avenue, Willowbranch Avenue, and Rubel Street in Jacksonville, Duval County, Florida. The site is bordered to the north by Lenox Avenue, to the east by McDuff Avenue South, to the south by Myra Street, and to the west by Comet Street and Lenox Avenue. The general site location is shown on Figure 1.

2.2 SITE CONDITIONS

At the time of our exploration, the site was developed as residential, asphalt roadways. The roads were two lanes with curb and gutter along both sides of the roads. Various underground and overhead utilities are located within the roadway corridor. Surface water was not observed near planned structural areas at the time of our exploration.

2.3 PROJECT DESCRIPTION

You provided project information via several discussions and an email dated May 8, 2020. We were provided with a copy of a site plan for the subject site, prepared by ETM, Inc. This plan indicated the boundary limits for the property, the existing roadways adjacent to and within the site, and the requested boring locations.

We understand the overall project will include understand approximately 37,000 linear feet of 2 inch, 4 inch 6 inch, and 8 inch diameter water main pipes. This report includes only the portions of the pipelines along portions of Nolan Street, Hunt Street, Edison Avenue, Lenox Avenue, Lenox Square, Gilmore Street, Ernest Street, Dellwood Street, Myra Street, Green Street, Plum Street, College Street, College Place, Luray Street, Jasmine Place, Melba Street, Soltice Street, Owen Avenue, Willowbranch Avenue, and Rubel Street referenced as Packages D-M covering approximately 32,598 linear feet of pipeline. The depth of the water main was not available to our office at the time of this report. Therefore, we have assumed the pipelines will be shallower than 10 feet below existing grades.

If project information varies from these conditions, then the recommendations in this report may need to be re-evaluated. We should be contacted if any of the above project information is incorrect so that we may reevaluate our recommendations.

3.0 FIELD EXPLORATION AND LABORATORY TESTING

3.1 FIELD EXPLORATION PROGRAM

We performed a field exploration between May 18, 2020 and May 22, 2020. The approximate boring locations are indicated on the attached Field Exploration Plan (Figure 3). Our personnel determined the boring locations using our handheld GPS receivers. The boring locations on the referenced Field Exploration Plan should be considered accurate only to the degree implied by the method of measurement used.

We located and performed 43 auger borings, drilled to depths of approximately 10 feet below the existing ground surface in general accordance with the methodology outlined in ASTM D 1452 to explore the subsurface conditions within the proposed pipeline areas. Representative soil samples also were recovered from the auger borings and returned to our laboratory for further evaluation. A summary of the field procedures is included in Appendix A.

3.2 LABORATORY TESTING

The laboratory testing performed by ECS for this project consisted of selected tests performed on samples obtained during our field exploration operations. The following paragraphs briefly discuss the results of the completed laboratory testing program.

An experienced geotechnical engineer visually classified each soil sample from the test borings on the basis of texture and plasticity in accordance with the AASHTO Soil Classification System in general accordance with ASTM D 2488. A Key to the Soil Classification System is included in Appendix A.

Selected samples of the soils encountered during the field exploration were subjected to quantitative laboratory testing to better define the composition of the soils encountered and to provide data for correlation to their anticipated strength and compressibility characteristics. The laboratory testing determined the moisture contents and particle size distributions of selected soil samples. The results of the laboratory testing are shown in the Laboratory Testing Summary included in Appendix B and summarized in the Roadway Soil Survey Sheet, Figure 2. Also, these results are shown on the Generalized Subsurface Profiles on Figures 4 through 11 and on the Log of Boring records at the respective depths from which the tested samples were recovered.

3.3 REGIONAL/SITE GEOLOGY

The study area is located within the Jacksonville Basin in Duval County, Florida. The near-surface geology consists of Plio-Pleistocene unconsolidated sands overlying Pliocene undifferentiated sandy clays/silts and clayey/silty sands. Below the undifferentiated sediments; sands, silts and clays of the Hawthorn Group are present. The Ocala Group (limestone) underlies the Hawthorn Group, and contains the Floridian aquifer. The Hawthorn Group acts as an aquiclude and separates the shallow water table from the Floridian aquifer within the Ocala Group and lower units.

The Hawthorn Group consists of a highly variable mixture of quartz sand, silt, clay, carbonates and phosphates, and is approximately 300 feet thick in the study area. The Hawthorn Group can be divided into three generalized units. The upper Hawthorn is primarily poorly consolidated dolomites and dolosilts with a mixture of clastics and phosphate. The middle unit is mostly clastic, and the lower unit is predominately dolomite. Occasionally, a lower unit of the Hawthorn will act as part of the Floridan aquifer. Beds of a single component (pure clay) do occur in the Hawthorn but are the exception to a widely varying lithology. Phosphate is nearly always present in the Hawthorn Group.

An unconformity exists between the Miocene Hawthorn Group and the overlying undifferentiated sandy clays and clayey sands from the Pliocene. These undifferentiated sediments often contain reworked phosphate from the Hawthorn near the contact. Shell beds and limestone ranging in thickness between approximately 10 and 20 feet were deposited on top of the Hawthorn in some areas prior to the major regression that occurred during late Miocene Period.

4.0 SUBSURFACE CHARACTERIZATION

The subsurface conditions encountered were generally consistent with published geological mapping. A graphical presentation of the generalized subsurface conditions is presented on Figures 4 through 11. Detailed boring records are included in Appendix A. It should be understood that the soil conditions will vary between the boring locations. The following table summarizes the soil conditions encountered.

4.1 SUBSURFACE STRATIGRAPHY

Table 4.1.1 Subsurface Stratigraphy

Approximate Depth Range (ft)	Stratum	Description
0 to 0.2-1.1	6	Asphalt and Limerock Base
0.5-1.1 to 1.5-8.5	1 and 2	Fine Sand (A-3) and Silty Fine Sand (A-2-4)
1.5-8.5 to 10	1, 2, 3, 4, and 5	Fine Sand (A-3), Silty Fine Sand (A-2-4), Clayey Fine Sand (A-2-6), Very Clayey Fine Sand (A-6), Clay with varying amount of sand (A-7-6)

Notes: (1) Standard Penetration Test

4.2 GROUNDWATER LEVEL

Measured Groundwater: Groundwater was encountered at each boring location and recorded at the time of drilling at depths varying from 3 feet to 8.5 feet below the existing ground surface. We note that groundwater levels will fluctuate due to seasonal climatic variations, surface water runoff patterns, construction operations, and other interrelated factors. The groundwater depth at each boring location is noted on the Generalized Subsurface Profiles and on the Log of Boring records.

Preliminary Estimated Seasonal High Groundwater: The normal seasonal high groundwater level is affected by a number of factors. The drainage characteristics of the soils, land surface elevation, relief points such as drainage ditches, lakes, rivers, swamp areas, etc., and distance to relief points are some of the more important factors influencing the seasonal high groundwater level.

Based on our interpretation of the site conditions, including the boring logs and Web Soil Survey, we estimate the normal seasonal high groundwater level at the site at the boring locations to be approximately at the depths shown on the Generalized Subsurface Profiles. It is possible that groundwater levels may exceed the estimated normal seasonal high groundwater level as a result of significant or prolonged rains.

5.0 DESIGN RECOMMENDATIONS

5.1 GENERAL

Our geotechnical engineering evaluation of the site and subsurface conditions at the property, with respect to the planned construction and our recommendations for site preparation and foundation support, are based on (1) our site observations, (2) the field and laboratory test data obtained, (3) our understanding of the project information as presented in this report, and (4) our experience with similar soil and loading conditions.

If the stated project information is incorrect, or should the location of the pipeline areas be changed, please contact us so that we can review our recommendations. Also, the discovery of any site or subsurface conditions during construction that deviate from the data obtained during this geotechnical exploration should also be reported to us for our evaluation.

The recommendations in the subsequent sections of this report present design and construction techniques that are appropriate for the planned construction. We recommend that ECS be provided the opportunity to review the foundation plans and earthwork specifications to verify that our recommendations have been properly interpreted and implemented.

5.2 PIPELINE SUPPORT RECOMMENDATIONS

In general, we consider the subsurface conditions at the site capable of supporting the proposed pipelines when constructed upon properly prepared subgrade soils. Unsuitable clayey soils (A-2-6, A-6, and A-7-6) encountered during excavation at the pipe invert elevations will require over-excavation and replacement with compacted suitable backfill soil. Provided the site preparation and earthwork construction recommendations outlined in Section 6.0 of this report are performed, the following parameters may be used for design.

5.2.1 Design Parameters

We anticipate the buried structures will exert little or no net downward pressure on the soils; rather, the structures may be subject to hydrostatic uplift pressure when the structures are empty. Below grade structures should be designed to resist lateral earth pressures and hydrostatic uplift pressures appropriate for their depth below existing grade and the normal seasonal high groundwater table.

The walls of the structures should be designed to resist at-rest lateral earth pressures, with equivalent fluid densities above and below the water table being as follows:

Above Water Table - Equivalent Fluid Density	60 pcf
Below Water Table - Equivalent Fluid Density	90 pcf

The above design values assume granular backfill around the pipelines. Lateral pressure distributions in accordance with the above do not take into account forces from construction equipment, wheel loads, or other surcharge loads.

5.2.2 Uplift Protection

When the water level within below-grade structures is maintained at or above the surrounding groundwater level, no net buoyancy will occur to the structure. However, a positive means of uplift protection may be necessary. Hydrostatic uplift forces can be resisted in several ways including:

1. Addition of dead weight to the structure.
2. Mobilizing the dead weight of the soil surrounding the structure.

At your request, we would be pleased to assist you in evaluating uplift protection requirements.

6.0 SITE CONSTRUCTION RECOMMENDATIONS

Site preparation as outlined in this section should be performed to provide more uniform foundation bearing conditions and to reduce the potential for post-construction settlements of the planned pipelines.

6.1 CLEARING

Prior to construction, the location of existing underground utility lines within the construction area should be established. Provisions should then be made to relocate interfering utilities to appropriate locations. It should be noted that if underground pipes are not properly removed or plugged, they may serve as conduits for subsurface erosion which may subsequently lead to excessive settlement of overlying pavement.

6.2 TEMPORARY GROUNDWATER CONTROL

The groundwater level was encountered in the borings at depths varying from 3 feet to 6.5 feet below the existing ground surface at the time of our exploration. Depending on the depth of excavation required for excavation to the pipeline bearing levels, and the potential need for over-excavation of clayey soils followed by compaction of the soils within the upper one foot below the exposed surface, it will be necessary to install temporary groundwater control measures to dewater the area to facilitate the excavation and compaction processes. The groundwater control measures should be determined by the contractor. The water table should be maintained at least 2 feet below the required depth of excavation. The dewatering system should not be decommissioned until sufficient deadweight exists on the structures to prevent uplift.

6.3 EXCAVATION SAFETY

All excavations and slopes should be made and maintained in accordance with OSHA excavation safety standards. The contractor is solely responsible for designing and constructing stable, temporary excavations and slopes and should shore, slope, or bench the sides of the excavations and slopes as required to maintain stability of both the excavation sides and bottom. The contractor's responsible person, as defined in 29 CFR Part 1926, should evaluate the soil exposed in the excavations as part of the contractor's safety procedures. In no case should slope height, slope inclination, or excavation depth, including utility trench excavation depth, exceed those specified in local, state, and federal safety regulations. ECS is providing this information solely as a service to our client. ECS is not assuming responsibility for construction site safety or the contractor's activities; such responsibility is not being implied and should not be inferred.

6.4 PREPARATION OF FOUNDATION SOILS

For those proposed pipelines which are anticipated to bear in sandy soils (A-3 and A-2-4), the soils should be excavated to the proposed bearing elevation and the exposed excavation surface should be compacted as outlined in Section 6.5. Once the pipe is installed, the trench should be backfilled with compacted structural backfill to final grade.

Several borings encountered clayey soils (A-2-6, A-6, and A-7-6). We recommend that these unsuitable soils be removed in accordance with Sections 103.2 and 104.3.1 of the *City of Jacksonville Standard Specifications for Roadway Construction*.

6.5 COMPACTION OF BOTTOM OF EXCAVATION

After installing the temporary groundwater control measures, and achieving the required depth of excavation, the exposed surface of sandy soils should be compacted by the use of hand-operated equipment. Typically, the material should exhibit moisture contents within ± 2 percentage points of the Modified Proctor optimum moisture content (AASHTO T-180) during the compaction operations. Compaction should continue until densities of at least 98 percent of the Modified Proctor maximum dry density (AASHTO T-180) have been achieved within the upper one foot below the exposed surface within the pipeline and manhole structures excavation.

If clayey soils are observed at the exposed surface, and the geotextile or flowable fill alternatives are chosen, then the bottom soils should be compacted to form a stable working surface. Otherwise, it is recommended the initial backfill layer be placed on top of the exposed (clayey soil) surface, then compacted.

Should the bearing level soils experience pumping and soil strength loss during the compaction operations, compaction work should be immediately terminated and (1) the disturbed soils removed and backfilled with dry structural fill soils which are then compacted, or (2) the excess moisture content within the disturbed soils allowed to dissipate before recompacting.

6.6 STRUCTURAL BACKFILL AND COMPACTION OF STRUCTURAL BACKFILL

Structural backfill within the pipeline excavation, and in areas in which over-excavation of unsuitable soils is required below the pipeline invert, should be placed in loose lifts not exceeding 6 inches in thickness and compacted by the use of hand-operated compaction equipment. However, structural backfill may be placed in loose lifts not exceeding 12 inches in thickness and compacted by the hand-operated compaction equipment at elevations greater than 12 inches above the top of pipe.

Structural backfill is defined as a non-plastic, inorganic, granular soil having less than 10 percent material passing the No. 200 mesh sieve and containing less than 4.0 percent organic material. The sandy soils (A-3, A-2-4) excavated for the structure may be used as backfill. Typically, the backfill material should exhibit moisture contents within ± 2 percent of the Modified Proctor optimum moisture content (AASHTO T-180) during the compaction operations. Compaction should continue until densities of at least 98 percent of the Modified Proctor maximum dry density (AASHTO T-180) have been achieved within each 6- or 12-inch-thick lift of the compacted structural backfill.

Because the clayey soils (A-2-6, A-6, and A-7-6) have excessive fines content, and a tendency to retain moisture which makes these soils may be very difficult to dry and compact, we recommend these soils not be used as structural backfill.

7.0 QUALITY CONTROL TESTING

ECS should be retained to perform the construction material testing and observations required for this project, to verify that our recommendations have been satisfied. We are the most qualified to address problems that may arise during construction, since we are familiar with the intent of our engineering design.

A representative number of field in-place density tests should be made in each lift of compacted backfill. Density tests are recommended to verify that satisfactory compaction operations have been performed. We recommend density testing be performed in accordance with JEA Standards and Specifications.

8.0 CLOSING

Our geotechnical exploration has been performed, our findings obtained, and our recommendations prepared, in accordance with generally accepted geotechnical engineering principles and practices. ECS is not responsible for any independent conclusions, interpretation, opinions, or recommendations made by others based on the data contained in this report.

Our scope of services was intended to evaluate the soil conditions within the zone of soil influenced by the pipeline system. Our scope of services does not address geologic conditions, such as sinkholes or soil conditions existing below the depth of the soil borings.

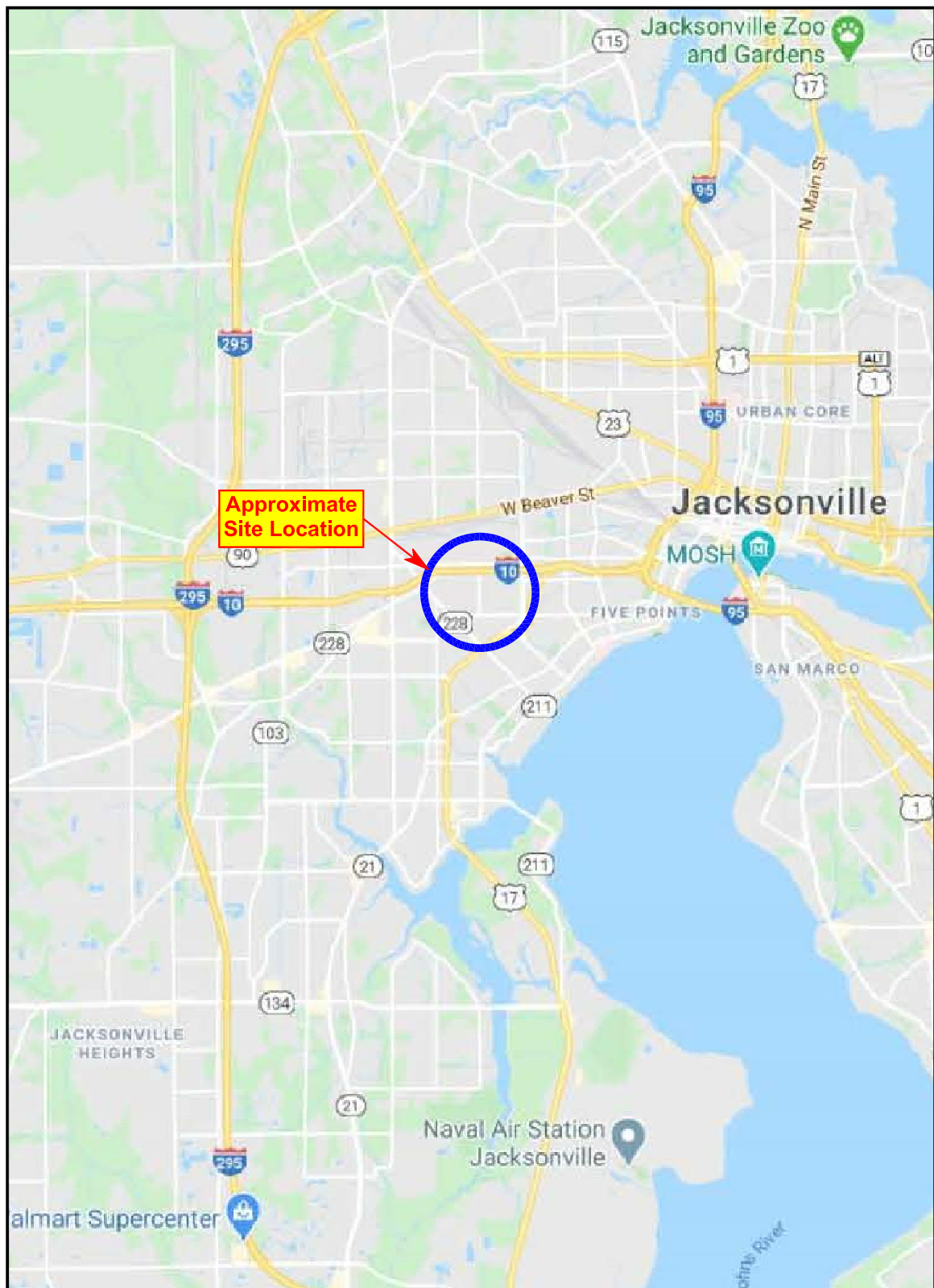
If any of the project description information discussed in this report is inaccurate, either due to our interpretation of the documents provided or site or design changes that may occur later, ECS should be contacted immediately in order that we can review the report in light of the changes and provide additional or alternate recommendations as may be required to reflect the proposed construction.

We recommend that ECS be allowed to review the project's plans and specifications pertaining to our work so that we may ascertain consistency of those plans/specifications with the intent of the geotechnical report.

Field observations, monitoring, and quality assurance testing during earthwork and foundation installation are an extension of and integral to the geotechnical design recommendation. We recommend that the owner retain these quality assurance services and that ECS be allowed to continue our involvement throughout these critical phases of construction to provide general consultation as issues arise. ECS is not responsible for the conclusions, opinions, or recommendations of others based on the data in this report.

FIGURES

- Figure 1 Site Location Plan
- Figure 2 Roadway Soil Survey Sheet
- Figure 3 Field Exploration Plan
- Figures 4-11 Generalized Subsurface Profiles



ECS Florida, LLC

Geotechnical ■ Construction Materials ■ Environmental ■ Facilities
 7064 Davis Creek Road, Jacksonville, FL 32256
 T: (904) 880-0960 • F: (904) 880-0970
www.ecslimited.com

Site Location Plan
JEA Galvanized Pipe
 Jacksonville, Florida



Date: 05/28/20

Project No.: 35-30388

Figure 1

JAS - 35-30388

DATE OF SURVEY: May 2020

SURVEY MADE BY: ECS Florida, LLC

SUBMITTED BY: -

SURVEY BEGINS STA. : -

SURVEY ENDS STA. : -

ROAD NO.: Varies

COUNTY: Duval

STRATUM NO.	ORGANIC CONTENT		MOISTURE CONTENT		SIEVE ANALYSIS RESULTS PERCENTAGE PASSING						ATTERBERG LIMITS (%)			SOIL CLASSIFICATION			DESCRIPTION
	NO. OF TESTS	% ORGANIC	NO. OF TESTS	% MOISTURE	NO. OF TESTS	10 MESH	40 MESH	60 MESH	100 MESH	200 MESH	NO. OF TESTS	LIQUID LIMIT	PLASTICITY INDEX	AASHTO GROUP	NO. OF TESTS	AASHTO LBR	
1	-	-	-	-	-	-	-	-	-	-	-	-	-	A-3	-	-	Fine SAND, Fine SAND With Silt, and Fine SAND With Clay
2	-	-	5	10-25	5	100	99-100	97-99	47-71	11-15	-	-	-	A-2-4	-	-	Silty Fine SAND, Fine SAND With Silt
3	-	-	8	19-29	8	99-100	98-100	98-99	56-85	17-31	-	-	-	A-2-6	-	-	Clayey Fine SAND
4	-	-	5	21-31	5	100	99-100	98-100	77-78	39-45	-	-	-	A-6	-	-	Very Clayey Fine SAND, Sandy CLAY
5	-	-	1	33	1	-	-	-	-	61	-	-	-	A-7-6	-	-	CLAY, CLAY With Sand
6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	Asphalt/Limerock

EMBANKMENT AND SUBGRADE MATERIAL

STRATA BOUNDARIES ARE APPROXIMATE MAKE FINAL CHECK AFTER GRADING

▼

GROUNDWATER LEVEL ENCOUNTERED AT TIME OF DRILLING

▽

ESTIMATED SEASONAL HIGH GROUNDWATER LEVEL

NOTES:

1. STRATA BOUNDARIES ARE APPROXIMATE AND REPRESENT ENCOUNTERED SOIL STRATA AT EACH TEST HOLE LOCATION ONLY. STRATUM CONNECTING LINES ARE SHOWN FOR ESTIMATING EARTHWORK ONLY AND DO NOT INDICATE ACTUAL STRATUM LIMITS. SUBSURFACE VARIATIONS BETWEEN BORINGS SHOULD BE ANTICIPATED AS INDICATED IN SECTION 3.0 OF OUR REPORT. FOR FURTHER DETAILS SEE FDOT STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION

2. STRATA 1 IS ACCEPTABLE SUBGRADE MATERIAL IN ACCORDANCE WITH SECTION 104.2 CITY OF JACKSONVILLE STANDARD SPECIFICATIONS FOR ROADWAY CONSTRUCTION.

3. STRATA 3, 4, AND 5 IS NOT SUITABLE FOR USE AS FILL MATERIAL IN ACCORDANCE WITH SECTION 103.4 CITY OF JACKSONVILLE STANDARD SPECIFICATIONS FOR ROADWAY CONSTRUCTION.

4. STRATA 3, 4, AND 5 ARE UNSUITABLE MATERIALS IN ACCORDANCE WITH SECTION 103.2 CITY OF JACKSONVILLE STANDARD SPECIFICATIONS FOR ROADWAY CONSTRUCTION. REMOVAL OF UNSUITABLE MATERIALS SHOULD BE PERFORMED IN ACCORDANCE WITH SECTIONS 103.2 AND 104.3.1 CITY OF JACKSONVILLE STANDARD SPECIFICATIONS FOR ROADWAY CONSTRUCTION.

5. THE SYMBOL "-" AN UNMEASURED PARAMETER.


DATE

DESCRIPTION

DATE

DESCRIPTION

DAVID W. SPANGLER, P.E.
P.E. LICENSE NUMBER 58770
ECS Florida, LLC
7064 DAVIS CREEK ROAD
JACKSONVILLE, FL 32256
CERTIFICATE OF AUTHORIZATION 26152



CITY OF JACKSONVILLE

ROAD NO.

COUNTY

ECS PROJECT NO.

Varies

DUVAL

35-30388

ROADWAY SOIL SURVEY SHEET

Sheet No.

-

JAS - 35-30388

THE OFFICIAL RECORD OF THIS SHEET IS THE ELECTRONIC FILE DIGITALLY SIGNED AND SEALED UNDER RULE 61G15-23.004, F.A.C.

Figure 2



LEGEND

▲ Approximate Location of Auger Boring

**ECS Florida, LLC**

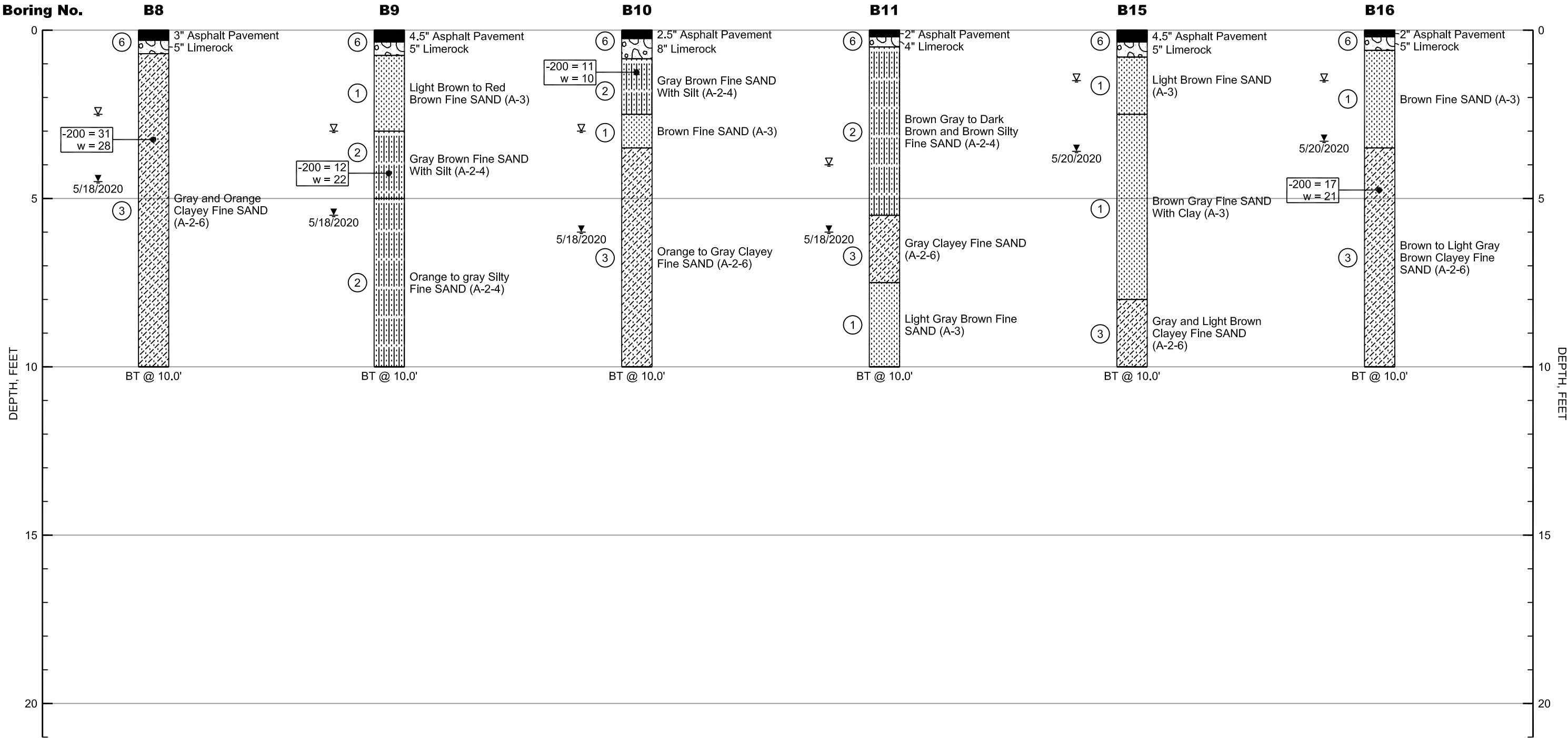
Geotechnical ■ Construction Materials ■ Environmental ■ Facilities
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T: (904) 880-0960 • F: (904) 880-0970
www.ecslimited.com

Field Exploration Plan
JEA Galvanized Pipe
Jacksonville, Florida

Date: 05/26/20

Project No.: 35-30388

Figure 3



LEGEND

- | | | |
|---|--|--|
| ⑥ Asphalt Pavement | ① Fine SAND, Fine SAND With Silt (A-3) | A-3 AASHTO Soil Classification System |
| ⑥ Limerock Base | ② Silty Fine SAND (A-2-4) | ▼ Groundwater Level at Time of Drilling |
| ③ Clayey Fine SAND (A-2-6) | ⑤ CLAY (A-7-6) | ▼ Estimated Normal Seasonal High Groundwater Level |
| ④ Very Clayey Fine SAND, Sandy CLAY (A-6) | ① Stratum Number (See Roadway Soil Survey Sheet) | -200 % Passing No. 200 U.S. Standard Sieve |
| BT Boring Terminated at Depth Below Grade | w Natural Moisture Content (%) | |

Generalized Subsurface Profiles

JEA Galvanized Pipe

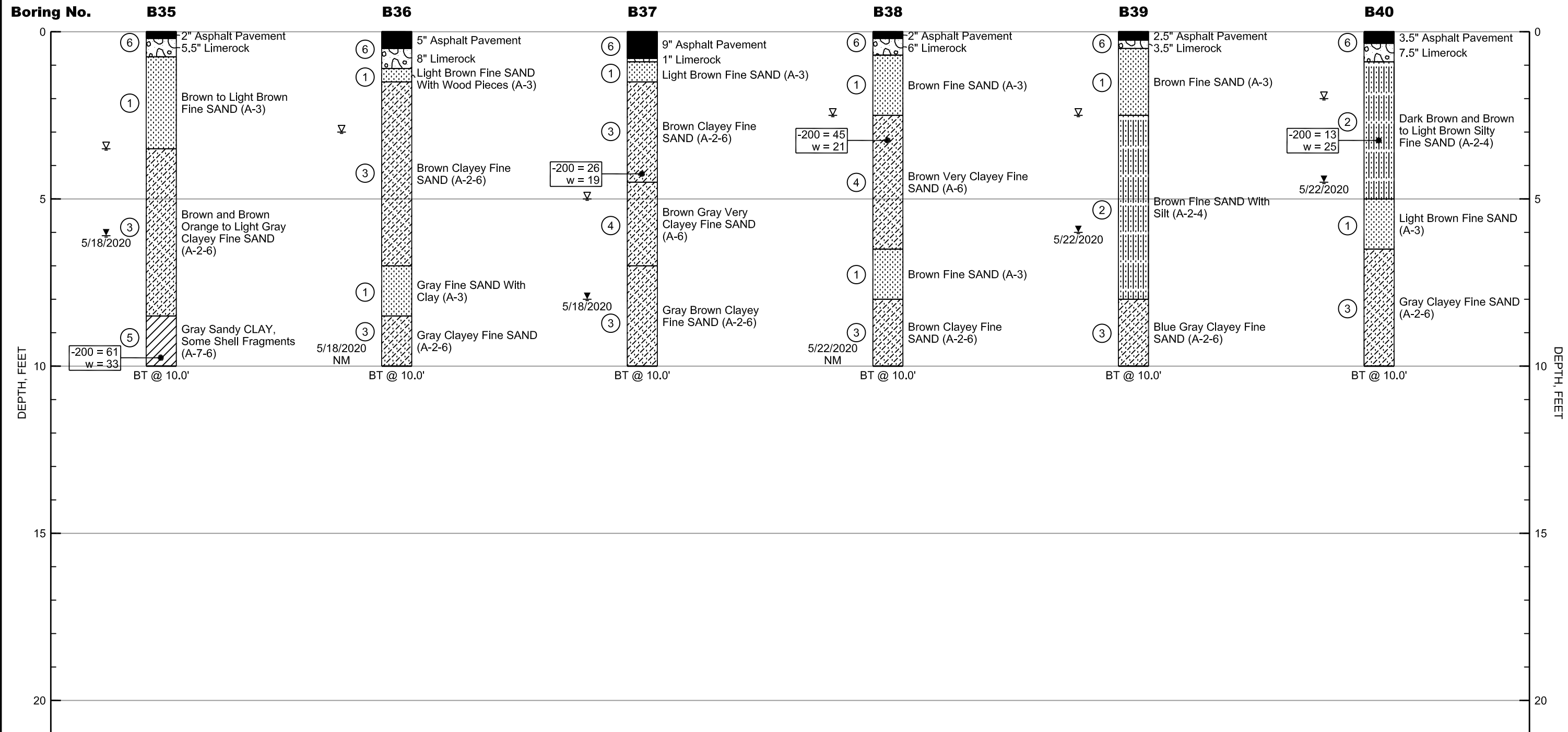
Jacksonville, Florida



DATE: 5/21/20

PROJ. NO.: 35-30388

Figure 4



LEGEND

- | | | | | | |
|---|---|--|--|------------------------------|--|
| ⑥ | Asphalt Pavement | ① | Fine SAND, Fine SAND With Silt (A-3) | A-3 | AASHTO Soil Classification System |
| ⑥ | Limerock Base | ② | Silty Fine SAND (A-2-4) | ▼ | Groundwater Level at Time of Drilling |
| ③ | Clayey Fine SAND (A-2-6) | ⑤ | CLAY (A-7-6) | ▽ | Estimated Normal Seasonal High Groundwater Level |
| ④ | Very Clayey Fine SAND, Sandy CLAY (A-6) | ① | Stratum Number (See Roadway Soil Survey Sheet) | -200 | % Passing No. 200 U.S. Standard Sieve |
| | BT | Boring Terminated at Depth Below Grade | w | Natural Moisture Content (%) | |

Generalized Subsurface Profiles

JEA Galvanized Pipe

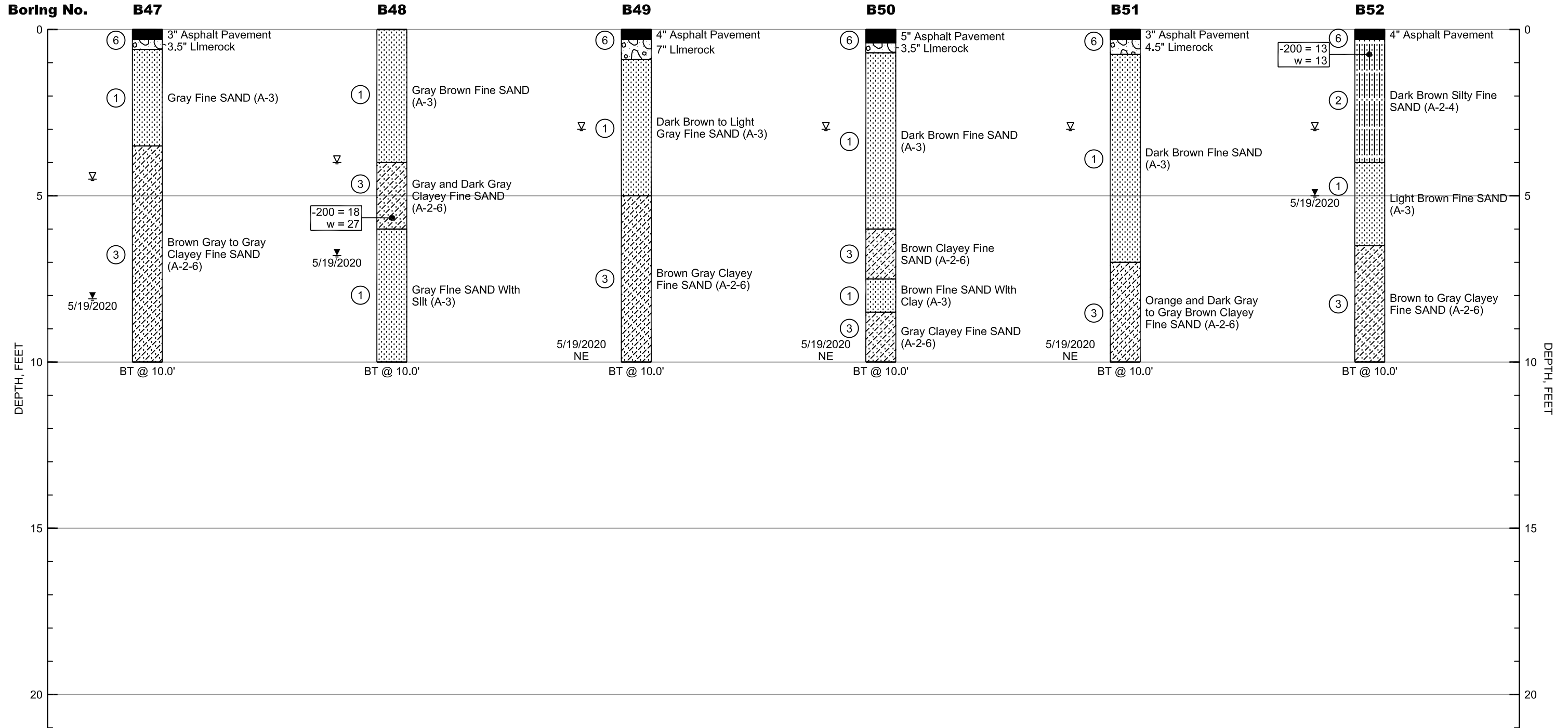
Jacksonville, Florida



DATE: 5/21/20

PROJ. NO.: 35-30388

Figure 8



LEGEND

- | | | |
|---|--|--|
| ⑥ Asphalt Pavement | ① Fine SAND, Fine SAND With Silt (A-3) | A-3 AASHTO Soil Classification System |
| ⑥ Limerock Base | ② Silty Fine SAND (A-2-4) | ▼ Groundwater Level at Time of Drilling |
| ③ Clayey Fine SAND (A-2-6) | ⑤ CLAY (A-7-6) | ▽ Estimated Normal Seasonal High Groundwater Level |
| ④ Very Clayey Fine SAND, Sandy CLAY (A-6) | ① Stratum Number (See Roadway Soil Survey Sheet) | -200 % Passing No. 200 U.S. Standard Sieve |
| BT Boring Terminated at Depth Below Grade | w Natural Moisture Content (%) | |

Generalized Subsurface Profiles

JEA Galvanized Pipe

Jacksonville, Florida

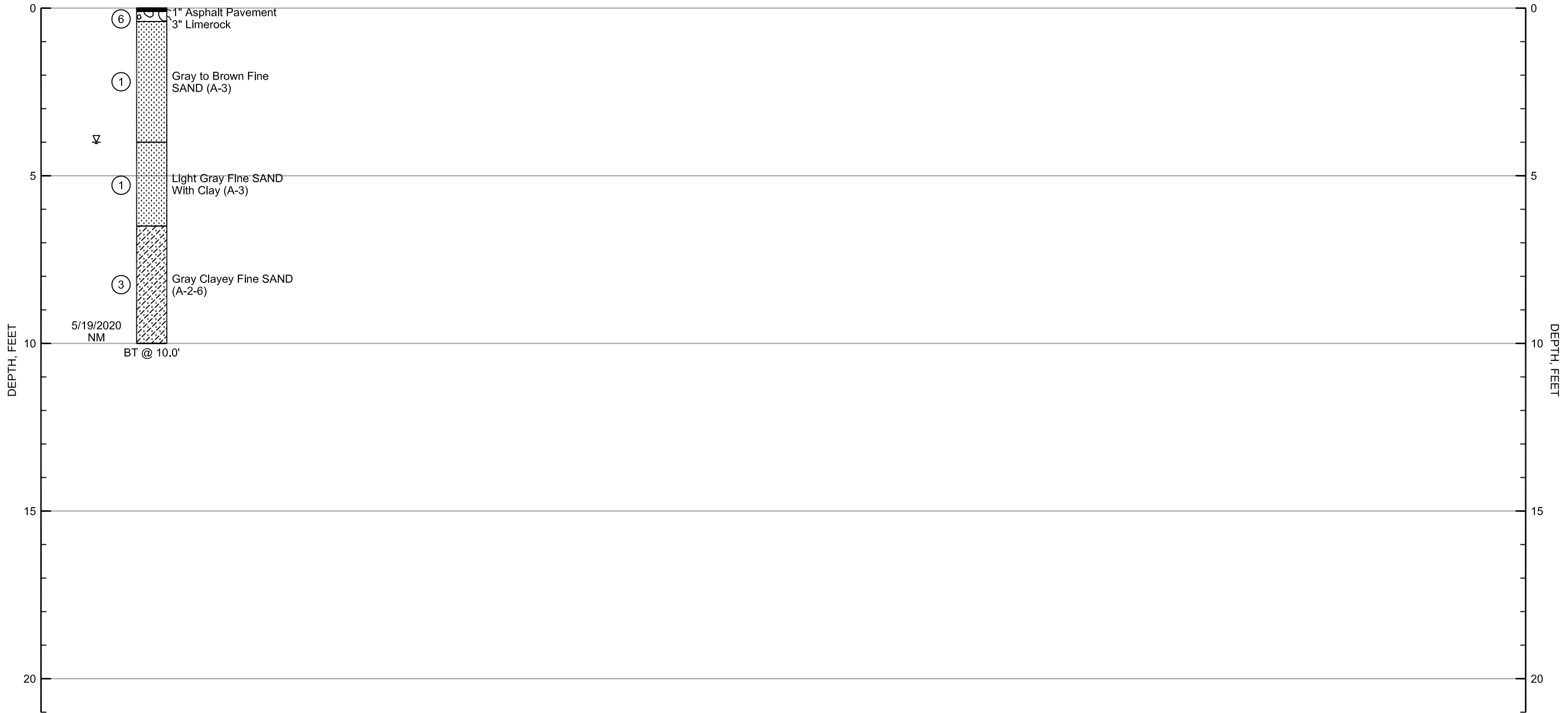


DATE: 5/21/20

PROJ. NO.: 35-30388

Figure 10

Boring No. **B53**



LEGEND

- | | | | | | |
|---|---|---|--|------|--|
| ⑥ | Asphalt Pavement | ① | Fine SAND, Fine SAND With Silt (A-3) | A-3 | AASHTO Soil Classification System |
| ⑥ | Limerock Base | ② | Silty Fine SAND (A-2-4) | ↘ | Groundwater Level at Time of Drilling |
| ③ | Clayey Fine SAND (A-2-6) | ⑤ | CLAY (A-7-6) | ↗ | Estimated Normal Seasonal High Groundwater Level |
| ④ | Very Clayey Fine SAND, Sandy CLAY (A-6) | ① | Stratum Number (See Roadway Soil Survey Sheet) | -200 | % Passing No. 200 U.S. Standard Sieve |
| | BT | | Boring Terminated at Depth Below Grade | w | Natural Moisture Content (%) |

Generalized Subsurface Profiles

JEA Galvanized Pipe

Jacksonville, Florida



DATE: 5/21/20

PROJ. NO.: 35-30388

Figure 11

APPENDIX A – Field Operations

Soil Boring Logs
Field Exploration Procedures
Key to Soil Classification

LOG OF BORING

LOG OF BORING

LOG OF BORING

LOG OF BORING



LOG OF BORING

Project No.: 35-30388
Boring No.: B20
Sheet 1 of 1

Project: JEA Galvanized Pipe Client: ET&M, Inc.
Boring Location: See Field Exploration Plan Drill Rig: 105T Driller: S. Burns
Groundwater Depth: NM Time: Drilling Date: 5/18/20 Drill Rod: Flight Auger Drill Mud:
Casing Size: Length of Casing:
Boring Begun: 5/18/20 Boring Completed: 5/18/20

SAMPLE NO.	DEPTH, FEET	SAMPLE TYPE	DESCRIPTION	BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE	PLASTIC LIMIT	MOISTURE CONTENT (%)	LIQUID LIMIT	SHEAR STRENGTH (ksf)	
											POCKET PENETROMETER UNDISTURBED SAMPLE	POCKET PENETROMETER DISTURBED SAMPLE
1	0		3" Asphalt Pavement									
			5" Limerock									
2	5		Brown Fine SAND (A-3)									
			Light Brown Clayey Fine SAND (A-2-6)									
3	10		Gray Fine SAND (A-3)									
			Boring Terminated @ 10 ft.									

Remarks NM = Groundwater Level Not Measured at Time of Drilling.

LOG OF BORING

LOG OF BORING

LOG OF BORING

LOG OF BORING



LOG OF BORING

Project No.: 35-30388
Boring No.: B36
Sheet 1 of 1

Project: JEA Galvanized Pipe Client: ET&M, Inc.
Boring Location: See Field Exploration Plan Drill Rig: 105T Driller: G. Uson
Groundwater Depth: NM Time: Drilling Date: 5/18/20 Drill Rod: Flight Auger Drill Mud:
Casing Size: Length of Casing:
Boring Begun: 5/18/20 Boring Completed: 5/18/20

SAMPLE NO.	DEPTH, FEET	SAMPLE TYPE	DESCRIPTION	BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE	PLASTIC LIMIT	MOISTURE CONTENT (%)	LIQUID LIMIT	SHEAR STRENGTH (ksf)	
											POCKET PENETROMETER UNDISTURBED SAMPLE	POCKET PENETROMETER DISTURBED SAMPLE
	0		5" Asphalt Pavement									
			8" Limerock									
1			Light Brown Fine SAND With Wood Pieces (A-3)									
			Brown Clayey Fine SAND (A-2-6)									
2												
3	5											
4												
5			Gray Fine SAND With Clay (A-3)									
6			Gray Clayey Fine SAND (A-2-6)									
	10		Boring Terminated @ 10 ft.									
	15											
	20											

Remarks NM = Groundwater Level Not Measured at Time of Drilling.



LOG OF BORING

Project No.: 35-30388
Boring No.: B38
Sheet 1 of 1

Project: JEA Galvanized Pipe Client: ET&M, Inc.
Boring Location: See Field Exploration Plan Drill Rig: 105T Driller: M. Letchworth
Groundwater Depth: NM Time: Drilling Date: 5/22/20 Casing Size: Drill Mud:
Boring Begun: 5/22/20 Boring Completed: 5/22/20

SAMPLE NO.	DEPTH, FEET	SAMPLE TYPE	DESCRIPTION	BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE	PLASTIC LIMIT	MOISTURE CONTENT (%)	LIQUID LIMIT	SHEAR STRENGTH (ksf)
	0		2" Asphalt Pavement								
			6" Limerock								
1			Brown Fine SAND (A-3)								
2			Brown Very Clayey Fine SAND (A-6)				45		+		
	5										
			Brown Fine SAND (A-3)								
3											
			Brown Clayey Fine SAND (A-2-6)								
4											
	10		Boring Terminated @ 10 ft.								
	15										
	20										

Remarks NM = Groundwater Level Not Measured at Time of Drilling.

LOG OF BORING

LOG OF BORING

LOG OF BORING

LOG OF BORING

LOG OF BORING



LOG OF BORING

Project No.: 35-30388
Boring No.: B49
Sheet 1 of 1

Project: JEA Galvanized Pipe Client: ET&M, Inc.
Boring Location: See Field Exploration Plan Drill Rig: 105T Driller: G. Uson
Groundwater Depth: NM Time: Drilling Date: 5/19/20 Drill Rod: Flight Auger Drill Mud:
Casing Size: Length of Casing:
Boring Begun: 5/19/20 Boring Completed: 5/19/20

SAMPLE NO.	DEPTH, FEET	SAMPLE TYPE	DESCRIPTION	BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE	PLASTIC LIMIT	MOISTURE CONTENT (%)	LIQUID LIMIT	SHEAR STRENGTH (ksf)	
											Unconfined Compression	Triaxial Compression
1	0		4" Asphalt Pavement									
			7" Limerock									
2			Dark Brown Fine SAND (A-3)									
			Light Gray Fine SAND (A-3)									
3	5		Brown Gray Clayey Fine SAND (A-2-6)									
4	10		Boring Terminated @ 10 ft.									
	15											
	20											

Remarks NM = Groundwater Level Not Measured at Time of Drilling.



LOG OF BORING

Project No.: 35-30388
Boring No.: B50
Sheet 1 of 1

Project: JEA Galvanized Pipe Client: ET&M, Inc.
Boring Location: See Field Exploration Plan Drill Rig: 105T Driller: G. Uson
Groundwater Depth: NM Time: Drilling Date: 5/19/20 Drill Rod: Flight Auger Drill Mud:
Casing Size: Length of Casing:
Boring Begun: 5/19/20 Boring Completed: 5/19/20

SAMPLE NO.	DEPTH, FEET	SAMPLE TYPE	DESCRIPTION	BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE	PLASTIC LIMIT	MOISTURE CONTENT (%)	LIQUID LIMIT	SHEAR STRENGTH (ksf)
1	0		5" Asphalt Pavement								
			3.5" Limerock								
			Dark Brown Fine SAND (A-3)								
2											
	5										
3			Brown Clayey Fine SAND (A-2-6)								
4			Brown Fine SAND With Clay (A-3)								
5			Gray Clayey Fine SAND (A-2-6)								
	10		Boring Terminated @ 10 ft.								
	15										
	20										

Remarks NM = Groundwater Level Not Measured at Time of Drilling.



LOG OF BORING

Project No.: 35-30388
Boring No.: B51
Sheet 1 of 1

Project: JEA Galvanized Pipe Client: ET&M, Inc.
Drill Rig: 105T Driller: G. Uson
Boring Location: See Field Exploration Plan Drill Rod: Flight Auger Drill Mud:
Casing Size: Length of Casing:
Groundwater Depth: NM Time: Drilling Date: 5/19/20 Boring Begun: 5/19/20 Boring Completed: 5/19/20

SAMPLE NO.	DEPTH, FEET	SAMPLE TYPE	DESCRIPTION	BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE	PLASTIC LIMIT	MOISTURE CONTENT (%)	LIQUID LIMIT	SHEAR STRENGTH (ksf)
1	0		3" Asphalt Pavement								<div><div></div> Pocket Penetrometer Undisturbed Sample</div> <div><div></div> Pocket Penetrometer Disturbed Sample</div> <div><div></div> Torvane</div> <div><div></div> Unconfined Compression</div> <div><div></div> Triaxial Compression</div>
			4.5" Limerock								
			Dark Brown Fine SAND (A-3)								
	5										
2			Orange and Dark Gray Clayey Fine SAND (A-2-6)								
3			Gray Brown Clayey Fine SAND (A-2-6)								
4											
	10		Boring Terminated @ 10 ft.								
	15										
	20										

Remarks NM = Groundwater Level Not Measured at Time of Drilling.



LOG OF BORING

Project No.: 35-30388
Boring No.: B53
Sheet 1 of 1

Project: JEA Galvanized Pipe Client: ET&M, Inc.
Boring Location: See Field Exploration Plan Drill Rig: 105T Driller: G. Uson
Groundwater Depth: NM Time: Drilling Date: 5/19/20 Drill Rod: Flight Auger Drill Mud:
Casing Size: Length of Casing:
Boring Begun: 5/19/20 Boring Completed: 5/19/20

SAMPLE NO.	DEPTH, FEET	SAMPLE TYPE	DESCRIPTION	BLOWS PER 6 IN.	N Value	PERCENT ORGANIC MATERIAL	PERCENT PASSING NO. 200 SIEVE	PLASTIC LIMIT	MOISTURE CONTENT (%)	LIQUID LIMIT	SHEAR STRENGTH (ksf)
1	0		1" Asphalt Pavement								
			3" Limerock								
			Gray Fine SAND (A-3)								
			Brown Fine SAND (A-3)								
2	5		Light Gray Fine SAND With Clay (A-3)								
3			Gray Clayey Fine SAND (A-2-6)								
4	10		Boring Terminated @ 10 ft.								
	15										
	20										

Remarks NM = Groundwater Level Not Measured at Time of Drilling.



FIELD EXPLORATION PROCEDURES

Flight Auger Boring

The auger borings were performed mechanically by the use of a continuous-flight auger attached to the drill rig and in general accordance with the latest revision of ASTM D 1452, "Soil Investigation and Sampling by Auger Borings". Representative samples of the soils brought to the ground surface by the augering process were placed in glass jars, sealed, and transported to our laboratory where they were examined by our engineer to verify the driller's field classification.



ECS FLORIDA, LLC

Geotechnical • Construction Materials • Environmental • Facilities

"Setting the Standard for Service"

KEY TO SOIL CLASSIFICATION

Description of Relative Density or Consistency in
Relation To Standard Penetration Resistance

<i>Granular Materials</i>		
Relative Density	Safety Hammer SPT N-Value (Blow/Foot)	Automatic Hammer SPT N-Value (Blow/Foot)
Very Loose	Less than 4	Less than 3
Loose	4 – 10	3 – 8
Medium Dense	10 – 30	8 – 24
Dense	30 – 50	24 – 40
Very Dense	Greater than 50	Greater than 40

<i>Silts and Clays</i>		
Consistency	Safety Hammer SPT N-Value (Blow/Foot)	Automatic Hammer SPT N-Value (Blow/Foot)
Very Soft	Less than 2	Less than 1
Soft	2 – 4	1 – 3
Firm	4 – 8	3 – 6
Stiff	8 – 15	6 – 12
Very Stiff	15 – 30	12 – 24
Hard	Greater than 30	Greater than 24

FDOT Classification of Highway Subgrade Materials (modified AASHTO classification)

General Classification	Granular Materials (35% or less passing No. 200)										Silt-clay materials (MORE THAN 35% PASSING NO. 200)							
Group Classification	A-3		A-2								A-4		A-5		A-6		A-7	
			A-2-4		A-2-5		A-2-6		A-2-7								A-7-5 A-7-6	
Sieve analysis, percent passing: No. 10 No. 40 No. 200	- 51 min. <5	- 51 min. 5 – 10	- - <12	- - 12 – 35	- - <12	- - 12 – 35	- - <12	- - 12 – 35	- - <12	- - 12 – 35	- - 36 – 50	- - >50	- - 36 – 50	- - >50	- - 36 – 50	- - >50	- - 36 – 50	- - >50
Characteristics of fraction passing No. 40: Liquid Limit Plasticity Index	- NP	- NP	40 max. 10 max.		41 min. 10 max.		40 max. 11 min.		41 min. 11 min.		40 max. 10 max.		41 min. 10 max.		40 max. 11 min.		41 min. 11 min.*	
Usual types of significant constituent materials	sand	sand w/silt or sand w/clay	sand w/silt	silty sand	sand w/silt or sand w/clay	silty sand or clayey sand	sand w/clay	clayey sand	sand w/clay	clayey sand	very silty sand	silt	very silty sand	silt	very clayey sand	clay	very clayey sand	clay

* Plasticity Index of A-7-5 subgroup is equal to or less than LL minus 30. Plasticity index of A-7-6 subgroup is greater than LL minus 30.

NOTE: Highly organic soils classify as A-8.

ORGANIC MATERIAL MODIFIERS	
Modifier	Organic Content
Trace	1% to 2%
Few	2% to 5%
Some	5% to 8%
Many	>8%

APPENDIX B – Laboratory Testing

Laboratory Testing Summary
Particle Size Distribution Reports
Laboratory Test Procedures

Laboratory Testing Summary

Page 1 of 2

Boring Number	Sample Number	Depth (feet)	MC1 (%)	Soil Type ²	Atterberg Limits ³			Percent Passing No. 200 Sieve ⁴	Moisture - Density (Corr.) ⁵		CBR Value ⁶	Other
					LL	PL	PI		Maximum Density (pcf)	Optimum Moisture (%)		
B8												
	2	3.50 - 4.00	28.0					30.9				
B9												
	3	3.50 - 4.00	22.1					11.8				
B10												
	1	1.00 - 1.50	9.5					10.8				
B16												
	3	4.00 - 4.50	21.2					16.8				
B19												
	2	2.00 - 2.50	18.5					25.1				
B22												
	3	4.50 - 5.00	30.7					43.2				
B23												
	5	7.50 - 8.00	22.6					26.9				
B26												
	3	4.50 - 5.00	25.9					44.9				
B30												
	3	7.50 - 8.00	25.0					15.1				
B31												
	4	8.00 - 8.50	25.7					31.4				
B33												
	1	1.00 - 1.50	25.4					40.4				
B35												
	6	8.50 - 9.00	33.3					60.6				
B37												
	2	3.5- - 4.00	19.1					25.7				
B38												
	2	3.00 - 3.50	21.3					44.8				

Notes:

1. ASTM D 2216, 2. ASTM D 2487, 3. ASTM D 4318, 4. ASTM D 1140, 5. See test reports for test method, 6. See test reports for test method

Definitions:

MC: Moisture Content, Soil Type: USCS (Unified Soil Classification System), LL: Liquid Limit, PL: Plastic Limit, PI: Plasticity Index, CBR: California Bearing Ratio, OC: Organic Content (ASTM D 2974)

Project No. 30388

Project Name: JEA Galvanized Pipe

Client: ETM (England-Thims & Miller Inc)

Printed On: Thursday, June 4, 2020



ECS Florida, LLC

Jacksonville, Florida

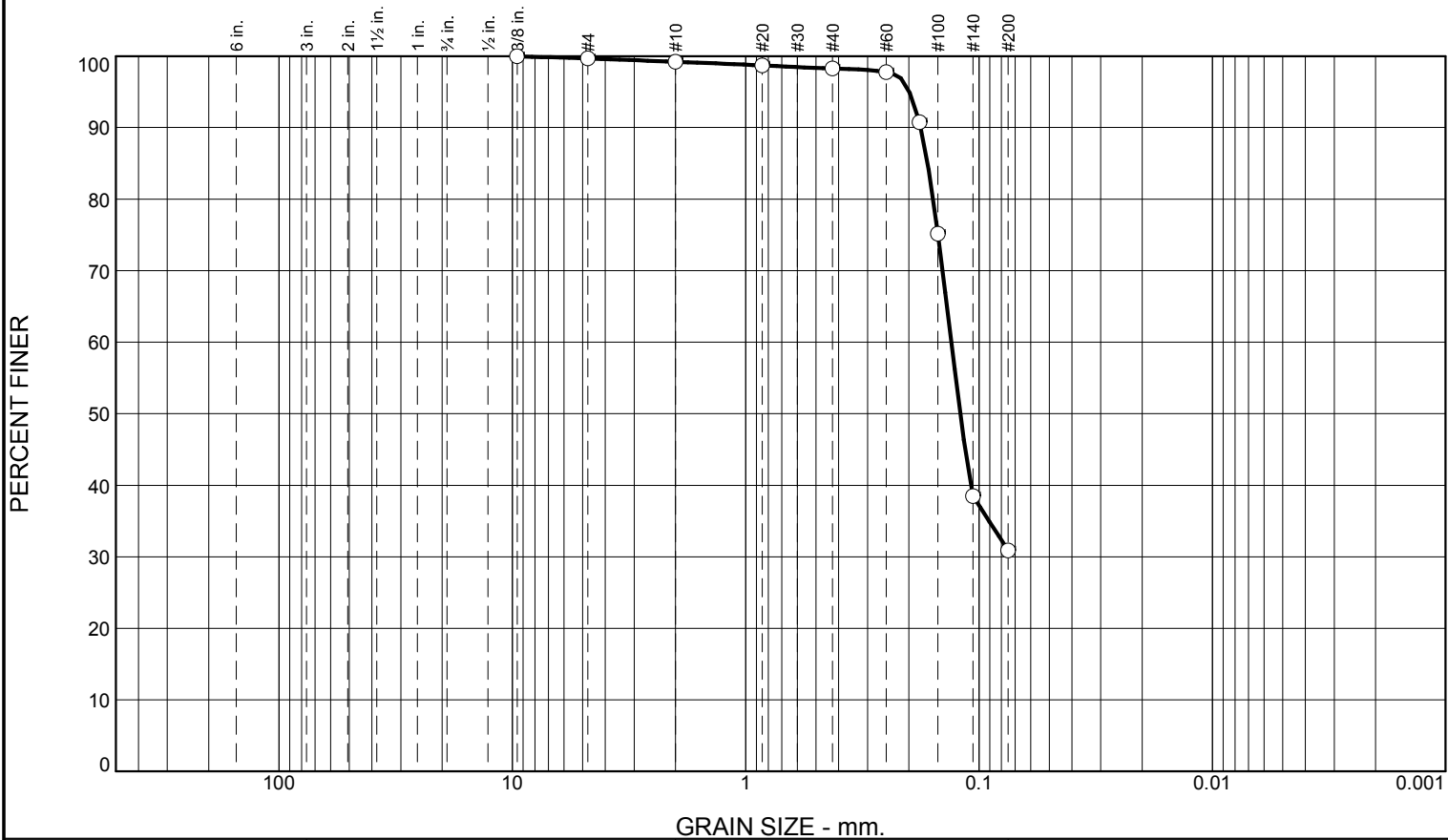
Page 2 of 2

Notes: 1. ASTM D 2216, 2. ASTM D 2487, 3. ASTM D 4318, 4. ASTM D 1140, 5. See test reports for test method, 6. See test reports for test method

Definitions: MC: Moisture Content, Soil Type: USCS (Unified Soil Classification System), LL: Liquid Limit, PL: Plastic Limit, PI: Plasticity Index, CBR: California Bearing Ratio, OC: Organic Content (ASTM D 2974)

Project No.	30388		ECS Florida, LLC
Project Name:	JEA Galvanized Pipe		
Client:	ETM (England-Thims & Miller Inc)		
Printed On:	Thursday, June 4, 2020		Jacksonville, Florida

Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0.0	0.8	0.9	67.4	30.9	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3/8"	100.0		
#4	99.7		
#10	99.2		
#20	98.7		
#40	98.3		
#60	97.8		
#80	90.8		
#100	75.2		
#140	38.5		
#200	30.9		

Material Description
Orange and Gray Clayey Sand

Atterberg Limits
 PL= LL= PI=

Coefficients
 D₉₀= 0.1777 D₈₅= 0.1661 D₆₀= 0.1314
 D₅₀= 0.1204 D₃₀= D₁₅=
 D₁₀= C_u= C_c=

Classification
 USCS= AASHTO= A-2-6

Remarks

* (no specification provided)

Source of Sample: B8
Sample Number: 2

Depth: 3.5

Date: 05-20-20



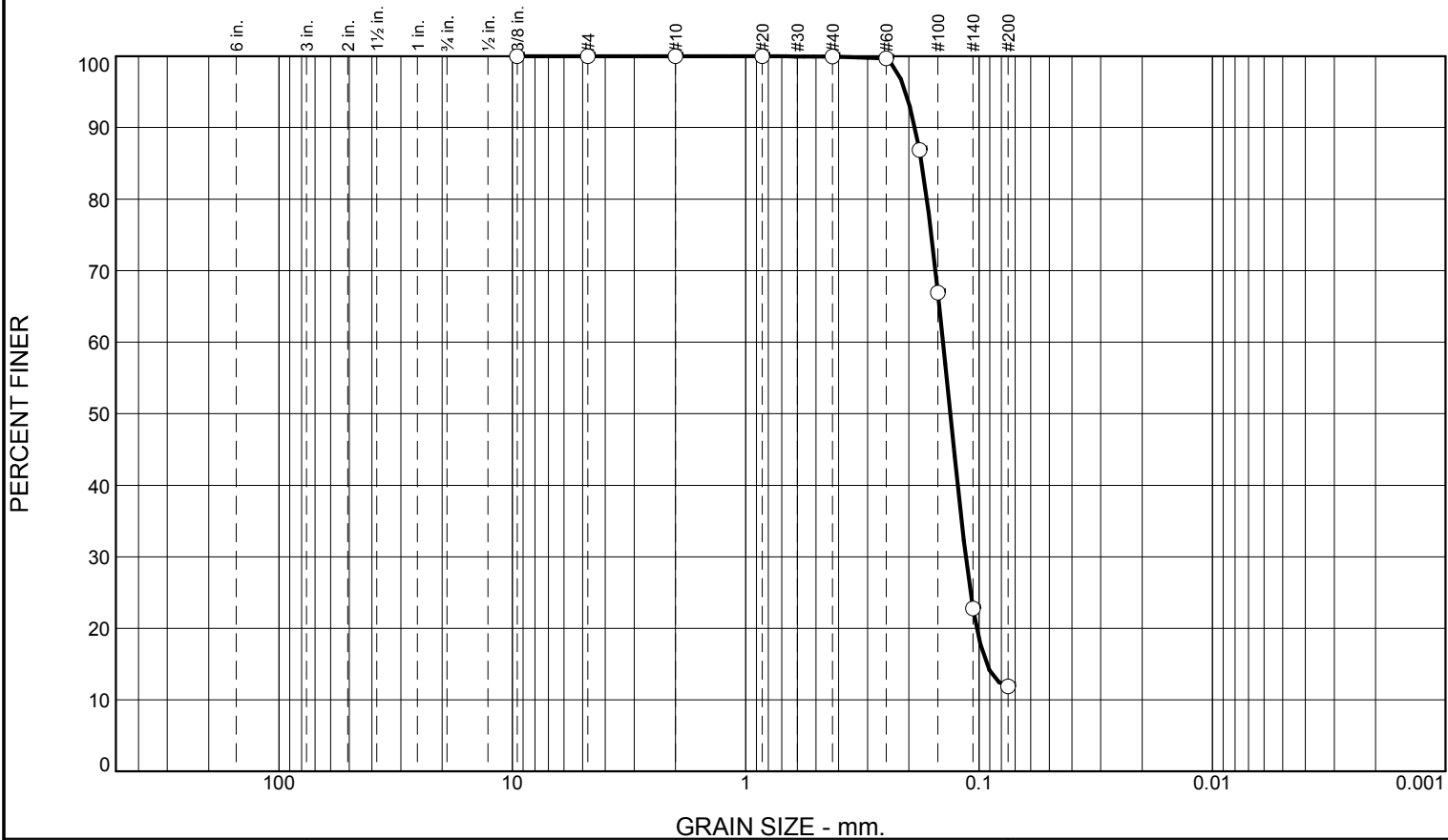
Client: ETM (England-Thims & Miller Inc)
Project: JEA Galvanized Pipe

Project No: 30388

Figure

Tested By: SC Checked By: JS

Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0.0	0.0	0.0	88.2	11.8	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3/8"	100.0		
#4	100.0		
#10	100.0		
#20	100.0		
#40	100.0		
#60	99.7		
#80	86.9		
#100	66.9		
#140	22.8		
#200	11.8		

* (no specification provided)

Material Description		
Gray Brown Sand with Silt		
<div> <div> Atterberg Limits PL= LL= PI= </div> <div> Coefficients D₉₀= 0.1876 D₈₅= 0.1761 D₆₀= 0.1425 D₅₀= 0.1328 D₃₀= 0.1140 D₁₅= 0.0927 D₁₀= C_u= C_c= </div> <div> Classification USCS= AASHTO= A-2-4 </div> <div> Remarks </div> </div>		

Source of Sample: B9
Sample Number: 3

Depth: 3.5

Date: 05-20-20



Client: ETM (England-Thims & Miller Inc)
Project: JEA Galvanized Pipe

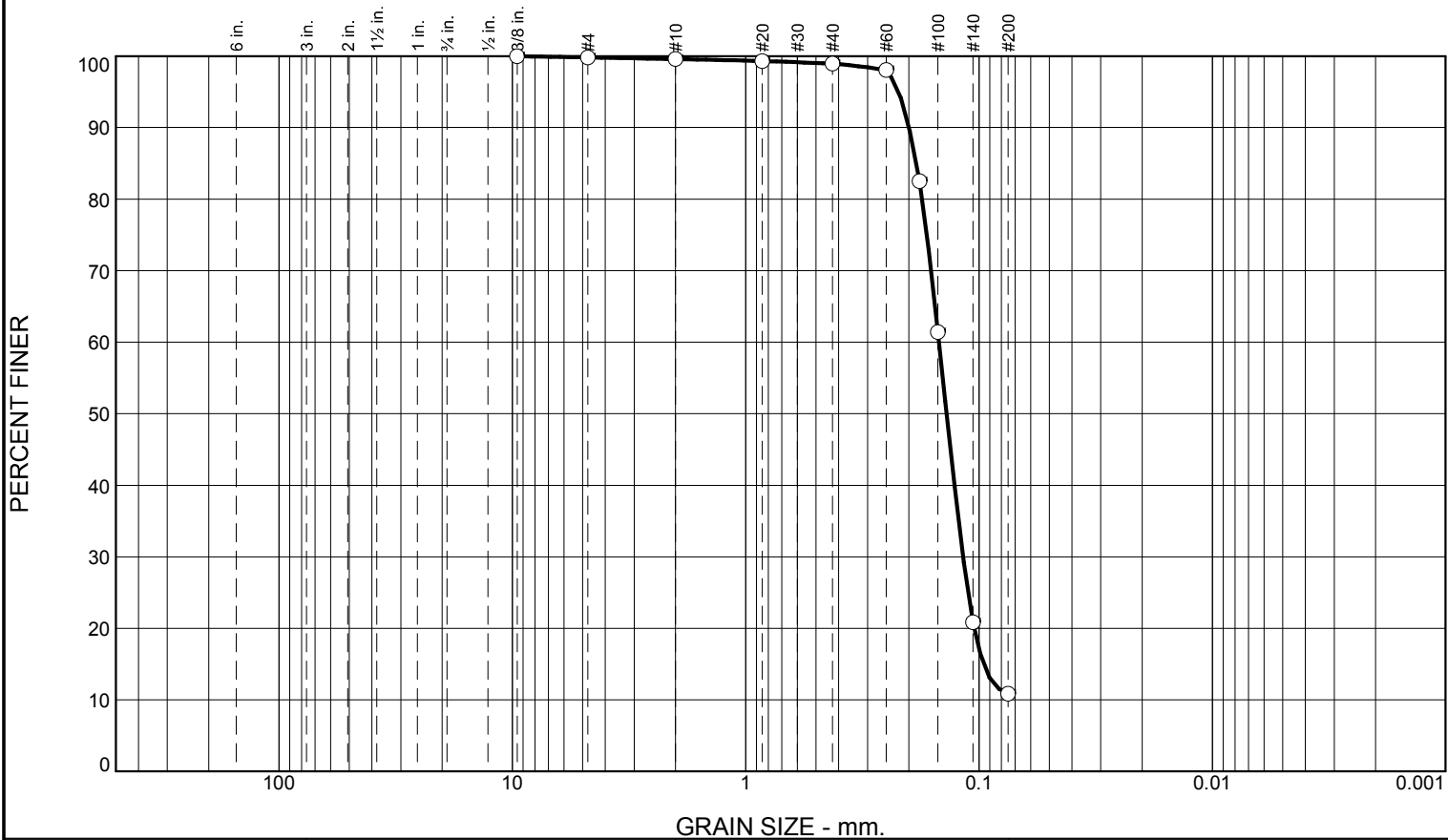
Project No: 30388

Figure

Tested By: SC

Checked By: JS

Particle Size Distribution Report



% +3"	% Gravel	% Sand		% Fines	
		Coarse	Fine	Silt	Clay
0.0	0.4	0.6	88.2	10.8	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3/8"	100.0		
#4	99.8		
#10	99.6		
#20	99.3		
#40	99.0		
#60	98.1		
#80	82.6		
#100	61.4		
#140	20.8		
#200	10.8		

* (no specification provided)

Material Description		
Brown and Gray Sand with Silt		
<div> <div> Atterberg Limits PL= LL= PI= </div> <div> Coefficients D₉₀= 0.1987 D₈₅= 0.1851 D₆₀= 0.1484 D₅₀= 0.1376 D₃₀= 0.1170 D₁₅= 0.0956 D₁₀= C_u= C_c= </div> <div> Classification USCS= AASHTO= A-2-4 </div> <div> Remarks </div> </div>		

Source of Sample: B10 Depth: 1
Sample Number: 1

Date: 05-20-20



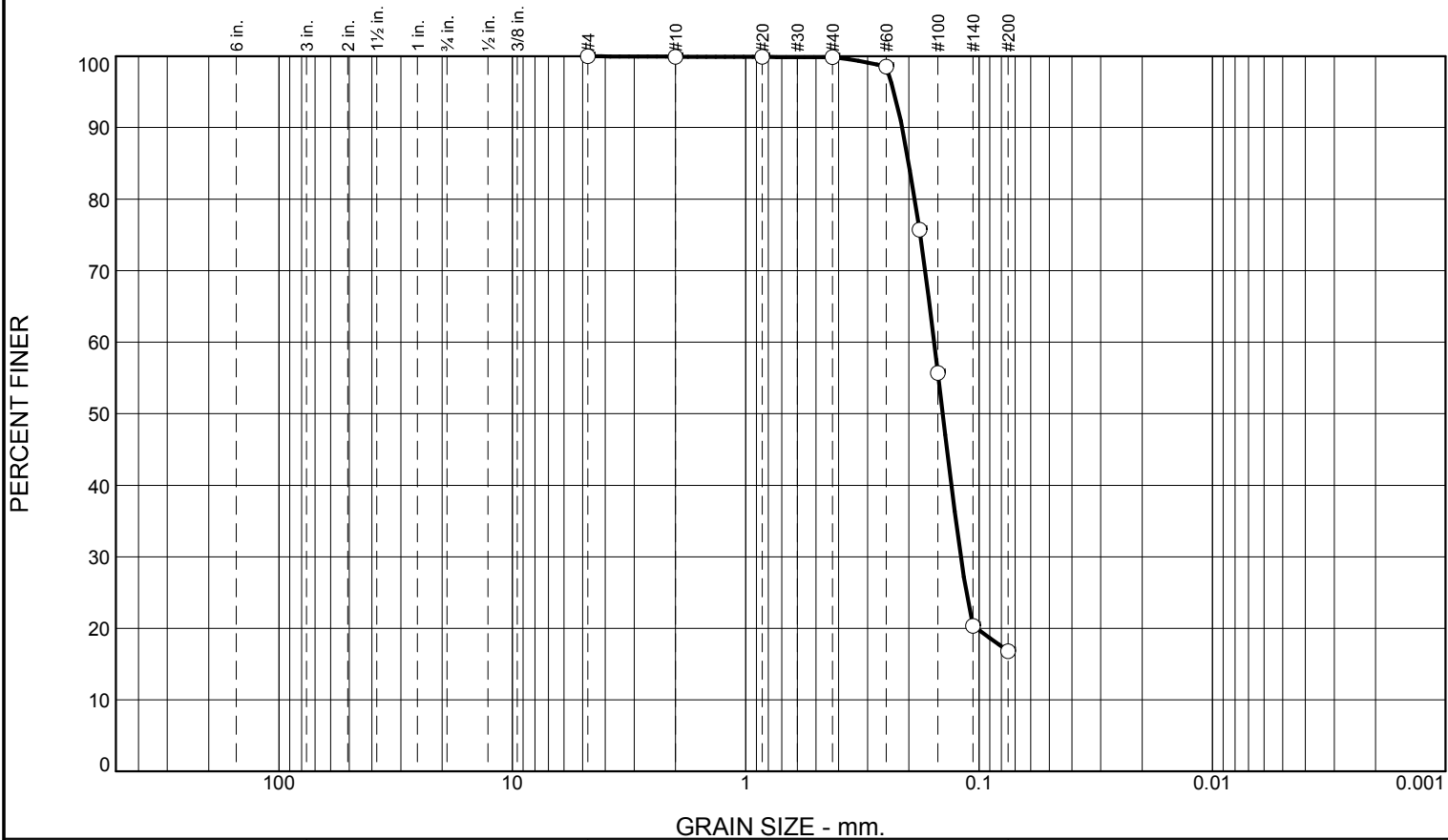
Client: ETM (England-Thims & Miller Inc)
Project: JEA Galvanized Pipe

Project No: 30388

Figure

Tested By: SC Checked By: JS

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.1	0.0	83.1	16.8	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.9		
#20	99.9		
#40	99.9		
#60	98.5		
#80	75.7		
#100	55.7		
#140	20.3		
#200	16.8		

Material Description
Brown Clayey Fine Sand

Atterberg Limits
 PL= LL= PI=

Coefficients
 D₉₀= 0.2132 D₈₅= 0.1995 D₆₀= 0.1556
 D₅₀= 0.1430 D₃₀= 0.1197 D₁₅=
 D₁₀= C_u= C_c=

Classification
 USCS= AASHTO= A-2-6

Remarks

* (no specification provided)

Source of Sample: B16 Depth: 4.00-6.00
 Sample Number: 3

Date:



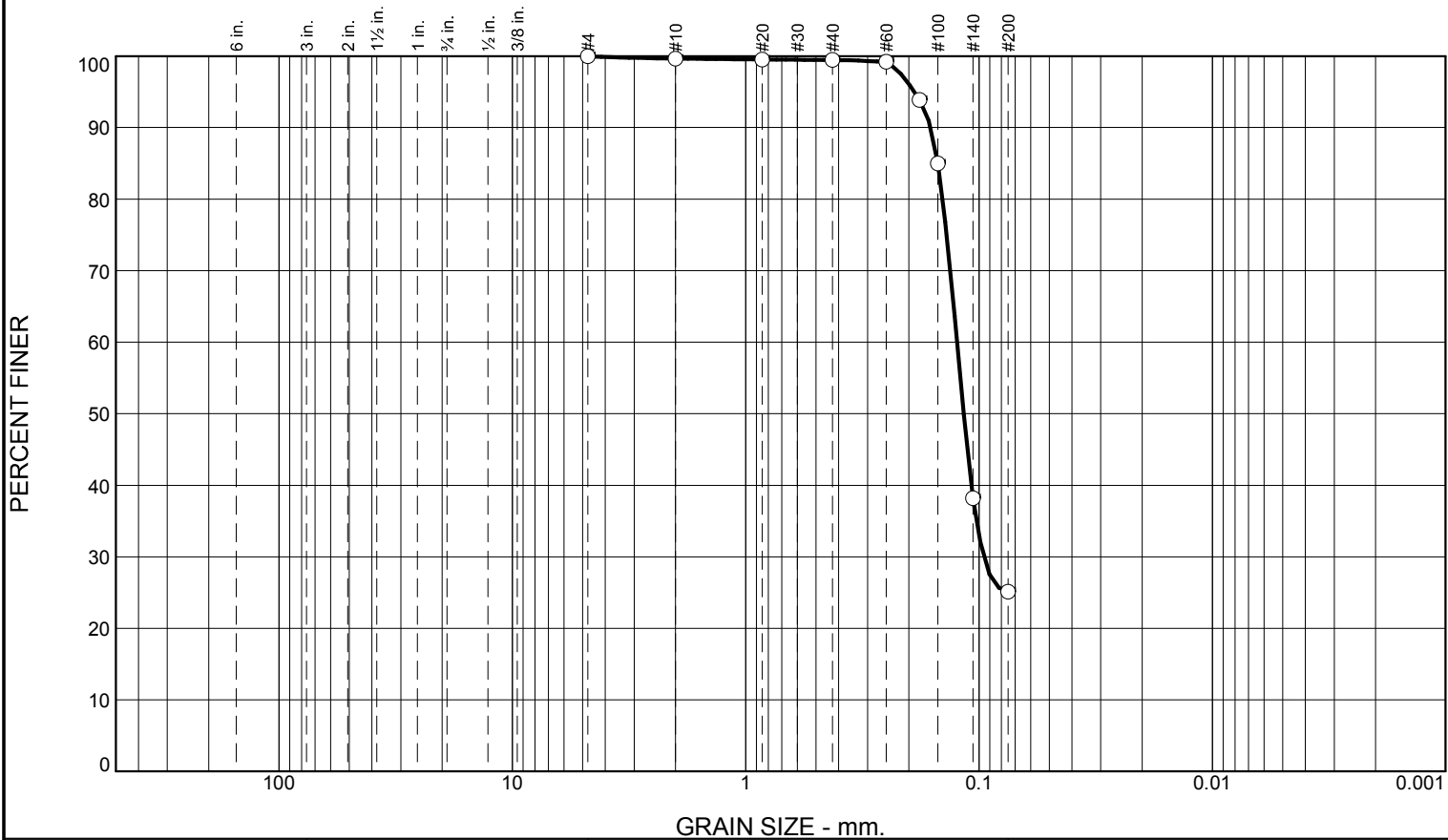
Client: ETM (England-Thims & Miller Inc)
 Project: JEA Galvanized Pipe

Project No: 30388

Figure

Tested By: SB Checked By: SB

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.3	0.2	74.4	25.1	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.7		
#20	99.6		
#40	99.5		
#60	99.2		
#80	93.9		
#100	85.0		
#140	38.2		
#200	25.1		

Material Description
Light Brown Clayey Fine Sand

Atterberg Limits
 PL= LL= PI=

Coefficients
 D₉₀= 0.1610 D₈₅= 0.1500 D₆₀= 0.1243
 D₅₀= 0.1163 D₃₀= 0.0954 D₁₅=
 D₁₀= C_u= C_c=

Classification
 USCS= AASHTO= A-2-6

Remarks

* (no specification provided)

Source of Sample: B19 Depth: 2.00-3.50
 Sample Number: 2

Date:



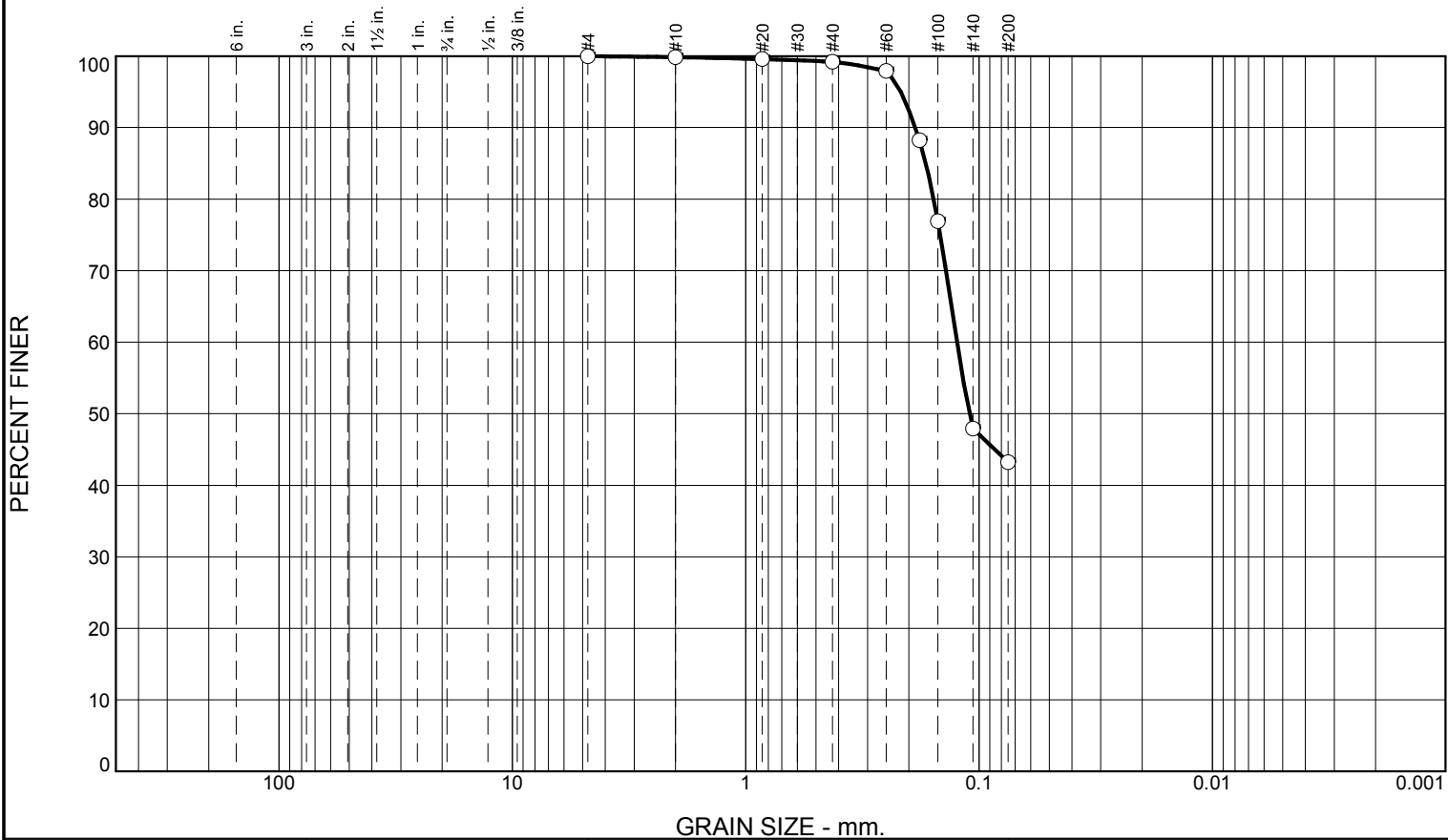
Client: ETM (England-Thims & Miller Inc)
 Project: JEA Galvanized Pipe

Project No: 30388

Figure

Tested By: SB Checked By: SB

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.1	0.7	56.0	43.2	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.9		
#20	99.6		
#40	99.2		
#60	97.9		
#80	88.3		
#100	76.9		
#140	47.9		
#200	43.2		

Material Description		
Gray Very Clayey Fine Sand		
Atterberg Limits		
PL=	LL=	PI=
Coefficients		
D ₉₀ = 0.1870	D ₈₅ = 0.1691	D ₆₀ = 0.1242
D ₅₀ = 0.1097	D ₃₀ =	D ₁₅ =
D ₁₀ =	C _u =	C _c =
Classification		
USCS=	AASHTO=	A-6
Remarks		

* (no specification provided)

Source of Sample: B22
Sample Number: 3

Depth: 4.50-7.00

Date:



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7064 Davis Creek Road
Jacksonville, Florida 32256
Phone: (904) 880-0960
Fax: (904) 880-0970

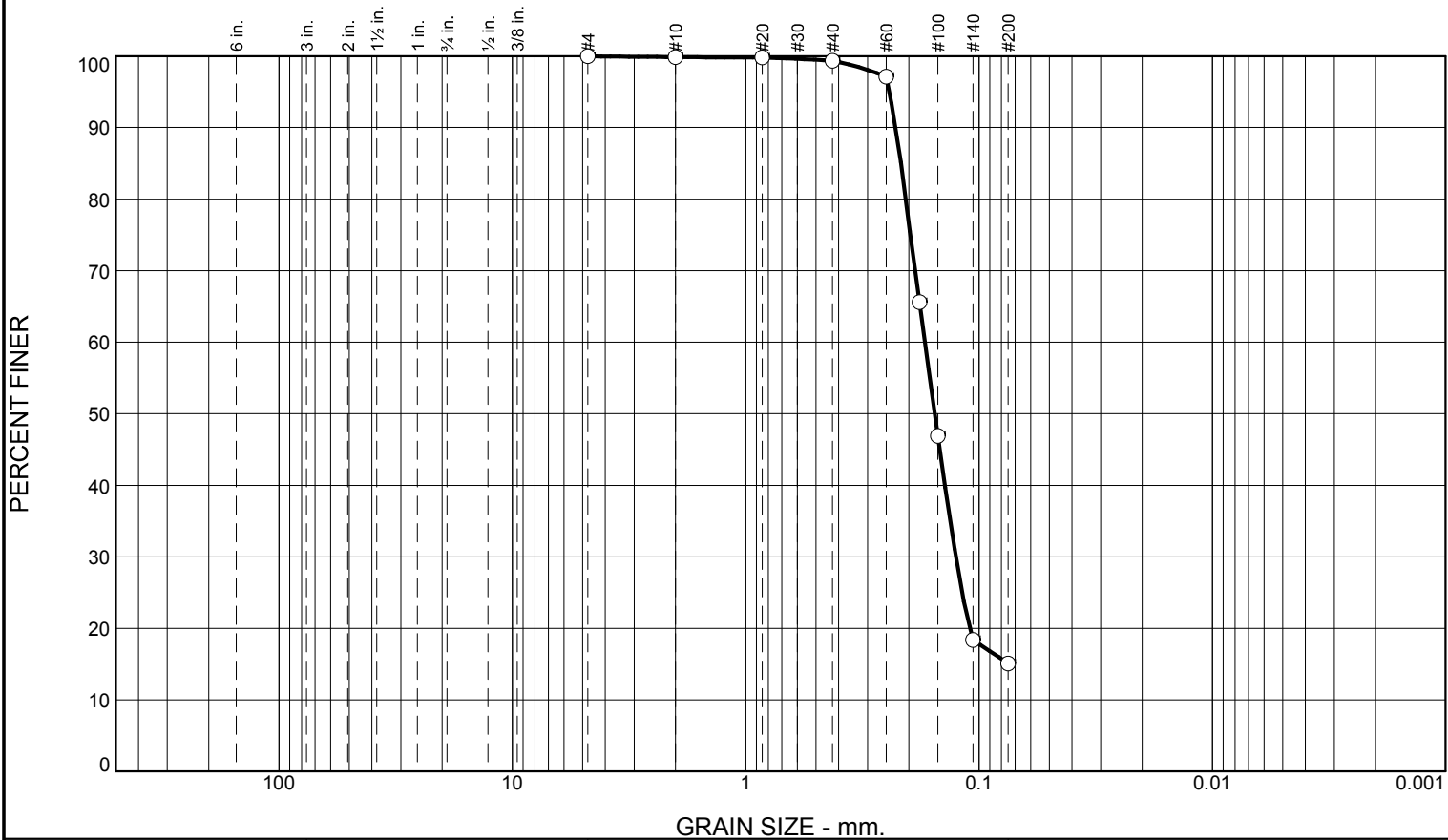
Client: ETM (England-Thims & Miller Inc)
Project: JEA Galvanized Pipe

Project No: 30388

Figure

Tested By: SB Checked By: SB

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.1	0.5	84.3	15.1	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.9		
#20	99.8		
#40	99.4		
#60	97.1		
#80	65.6		
#100	46.9		
#140	18.4		
#200	15.1		

Material Description		
Brown Silty Fine Sand		
Atterberg Limits		
PL=	LL=	PI=
Coefficients		
D ₉₀ = 0.2275	D ₈₅ = 0.2158	D ₆₀ = 0.1707
D ₅₀ = 0.1547	D ₃₀ = 0.1257	D ₁₅ =
D ₁₀ =	C _u =	C _c =
Classification		
USCS=	AASHTO=	A-2-4
Remarks		

* (no specification provided)

Source of Sample: B30 Depth: 7.50-9.00
Sample Number: 3

Date:



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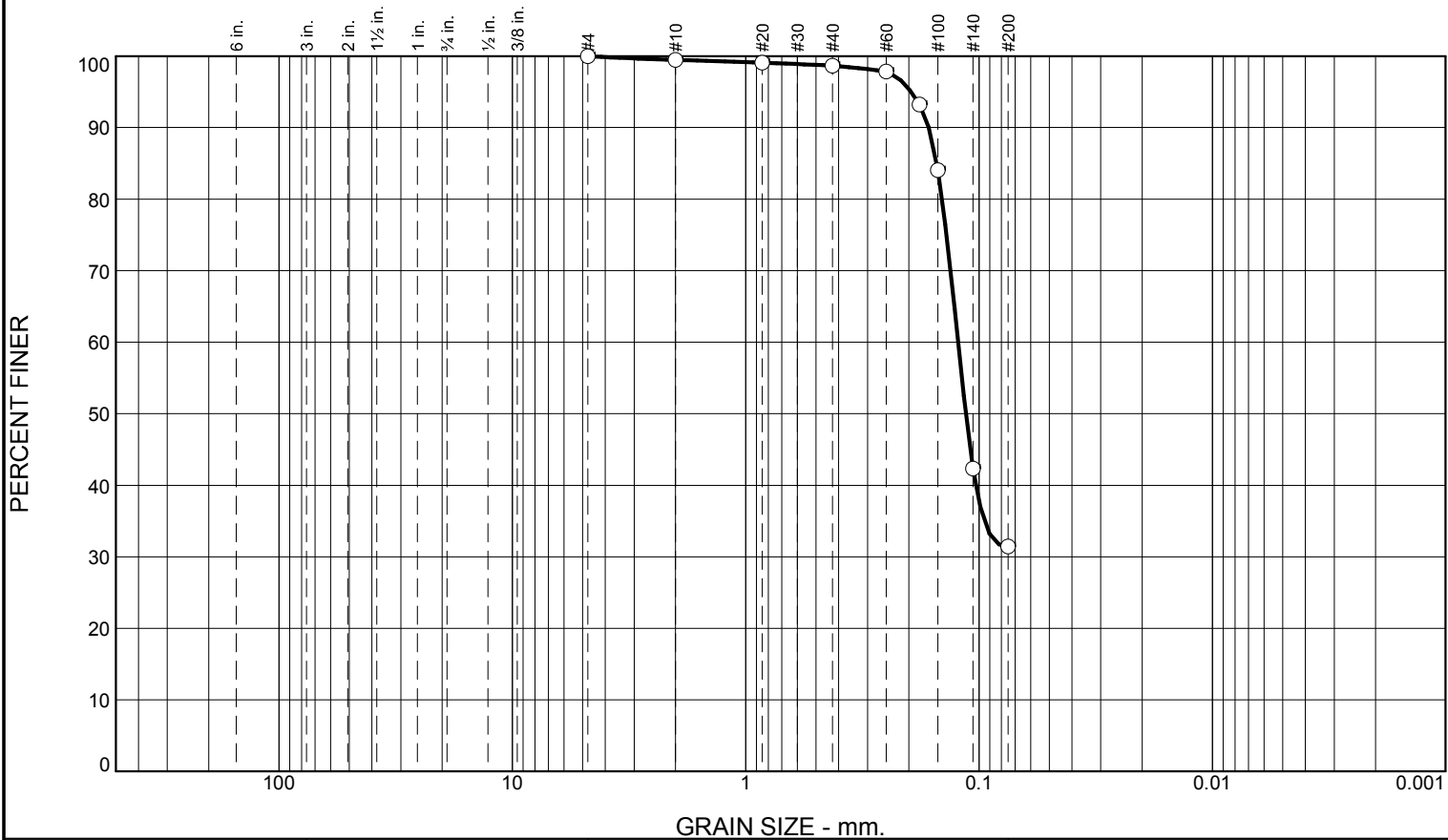
Client: ETM (England-Thims & Miller Inc)
Project: JEA Galvanized Pipe

Project No: 30388

Figure

Tested By: SB Checked By: SB

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.5	0.8	67.3	31.4	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.5		
#20	99.1		
#40	98.7		
#60	97.9		
#80	93.2		
#100	84.1		
#140	42.3		
#200	31.4		

Material Description		
Brown Gray Clayey Fine Sand		
Atterberg Limits		
PL=	LL=	PI=
Coefficients		
D ₉₀ = 0.1643	D ₈₅ = 0.1517	D ₆₀ = 0.1230
D ₅₀ = 0.1138	D ₃₀ =	D ₁₅ =
D ₁₀ =	C _u =	C _c =
Classification		
USCS=	AASHTO=	A-2-6
Remarks		

* (no specification provided)

Source of Sample: B31 Depth: 8.00-10.00
Sample Number: 4

Date:



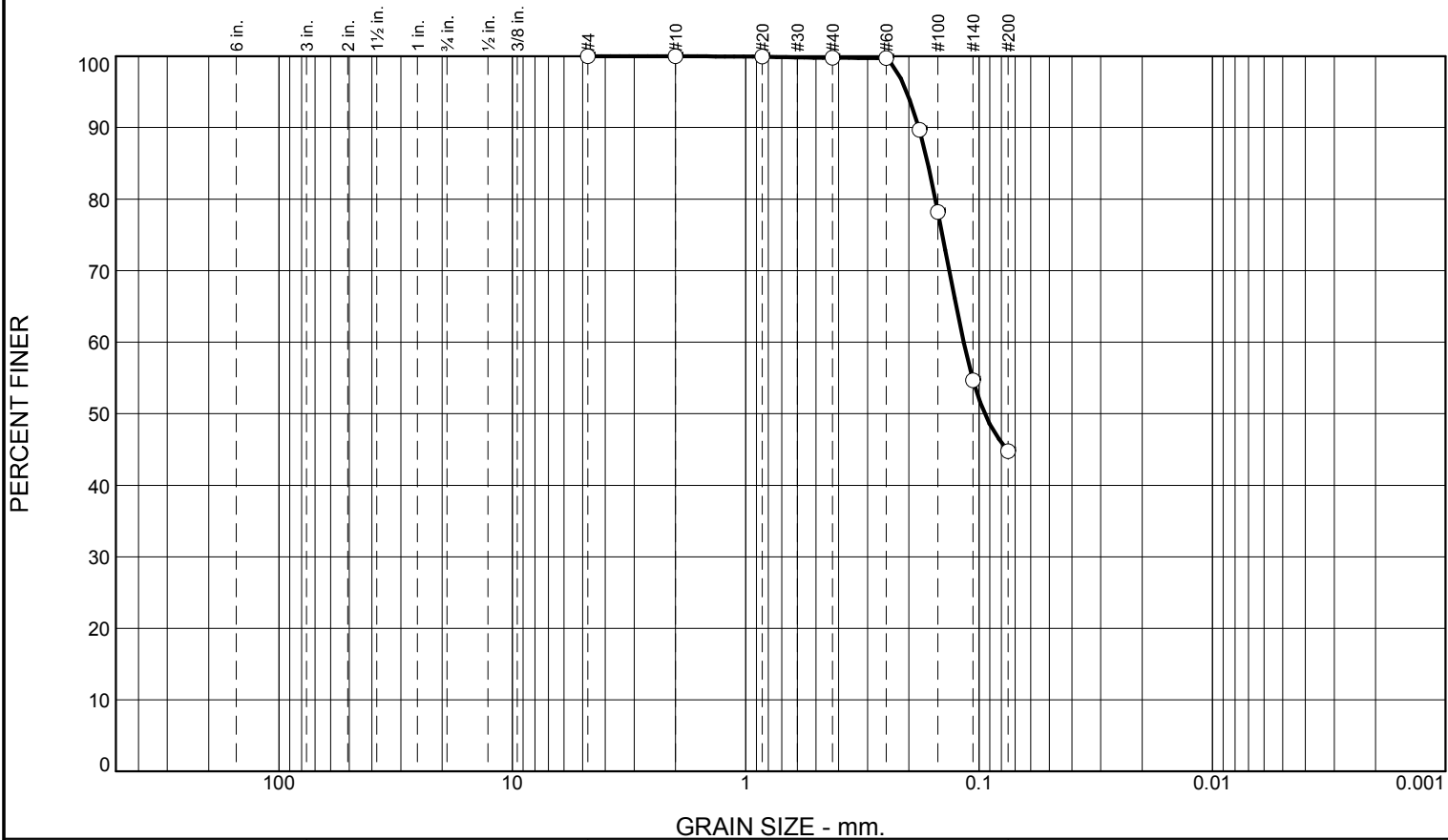
Client: ETM (England-Thims & Miller Inc)
Project: JEA Galvanized Pipe

Project No: 30388

Figure

Tested By: SB Checked By: SB

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.2	55.0	44.8	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	100.0		
#20	99.9		
#40	99.8		
#60	99.8		
#80	89.7		
#100	78.2		
#140	54.7		
#200	44.8		

Material Description
Brown Very Clayey Fine Sand

Atterberg Limits
 PL= LL= PI=

Coefficients
 D₉₀= 0.1810 D₈₅= 0.1658 D₆₀= 0.1163
 D₅₀= 0.0945 D₃₀= D₁₅=
 D₁₀= C_u= C_c=

Classification
 USCS= AASHTO= A-6

Remarks

* (no specification provided)

Source of Sample: B38 Depth: 2.00-3.50
 Sample Number: 2

Date:



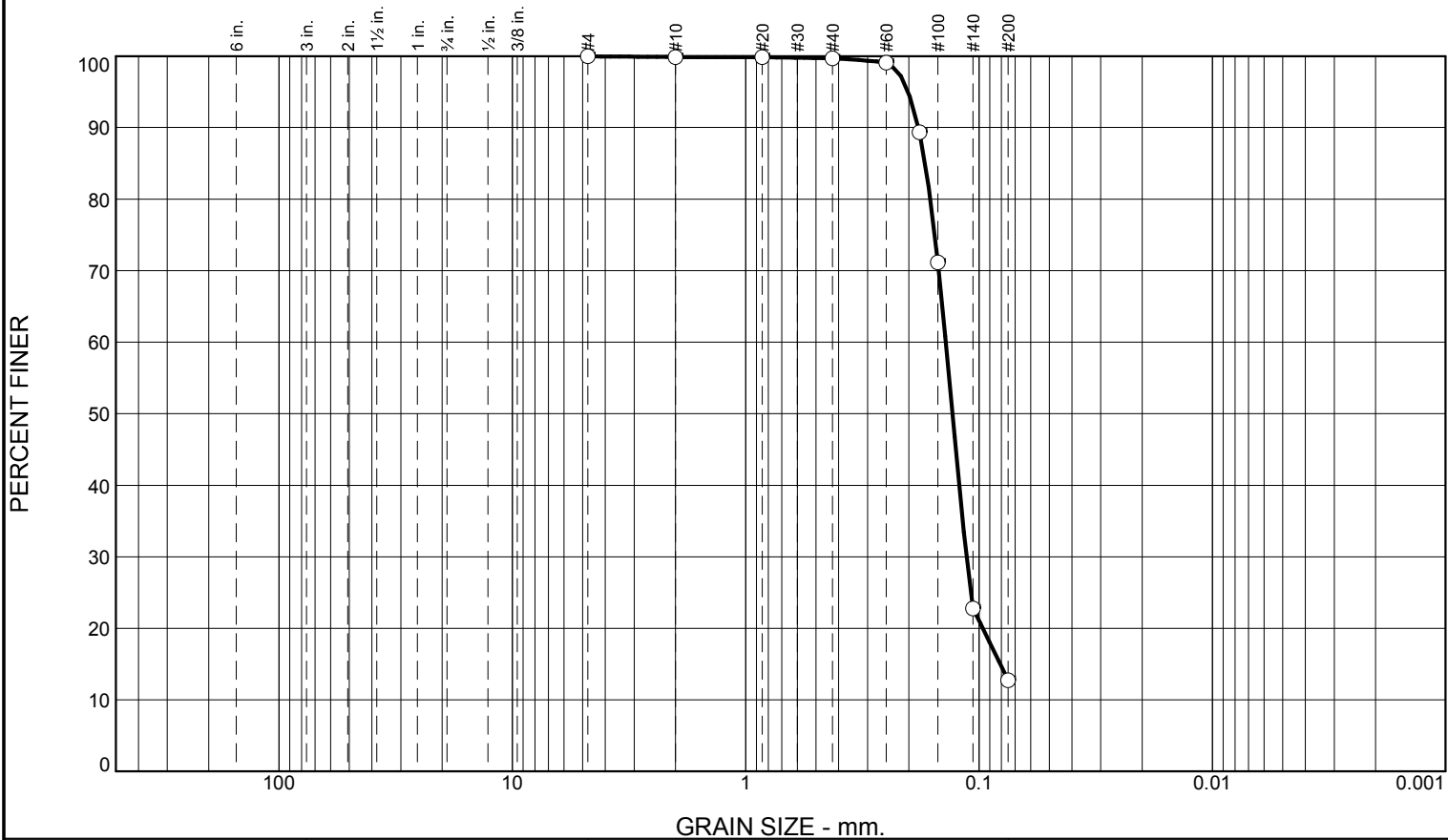
Client: ETM (England-Thims & Miller Inc)
 Project: JEA Galvanized Pipe

Project No: 30388

Figure

Tested By: SB Checked By: SB

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.1	0.2	87.0	12.7	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	99.9		
#20	99.9		
#40	99.7		
#60	99.1		
#80	89.4		
#100	71.2		
#140	22.8		
#200	12.7		

Material Description		
Brown Silty Fine Sand		
Atterberg Limits		
PL=	LL=	PI=
Coefficients		
D ₉₀ = 0.1817	D ₈₅ = 0.1702	D ₆₀ = 0.1387
D ₅₀ = 0.1300	D ₃₀ = 0.1132	D ₁₅ = 0.0811
D ₁₀ =	C _u =	C _c =
Classification		
USCS=	AASHTO=	A-2-4
Remarks		

* (no specification provided)

Source of Sample: B40 Depth: 2.00-3.50
Sample Number: 2

Date:



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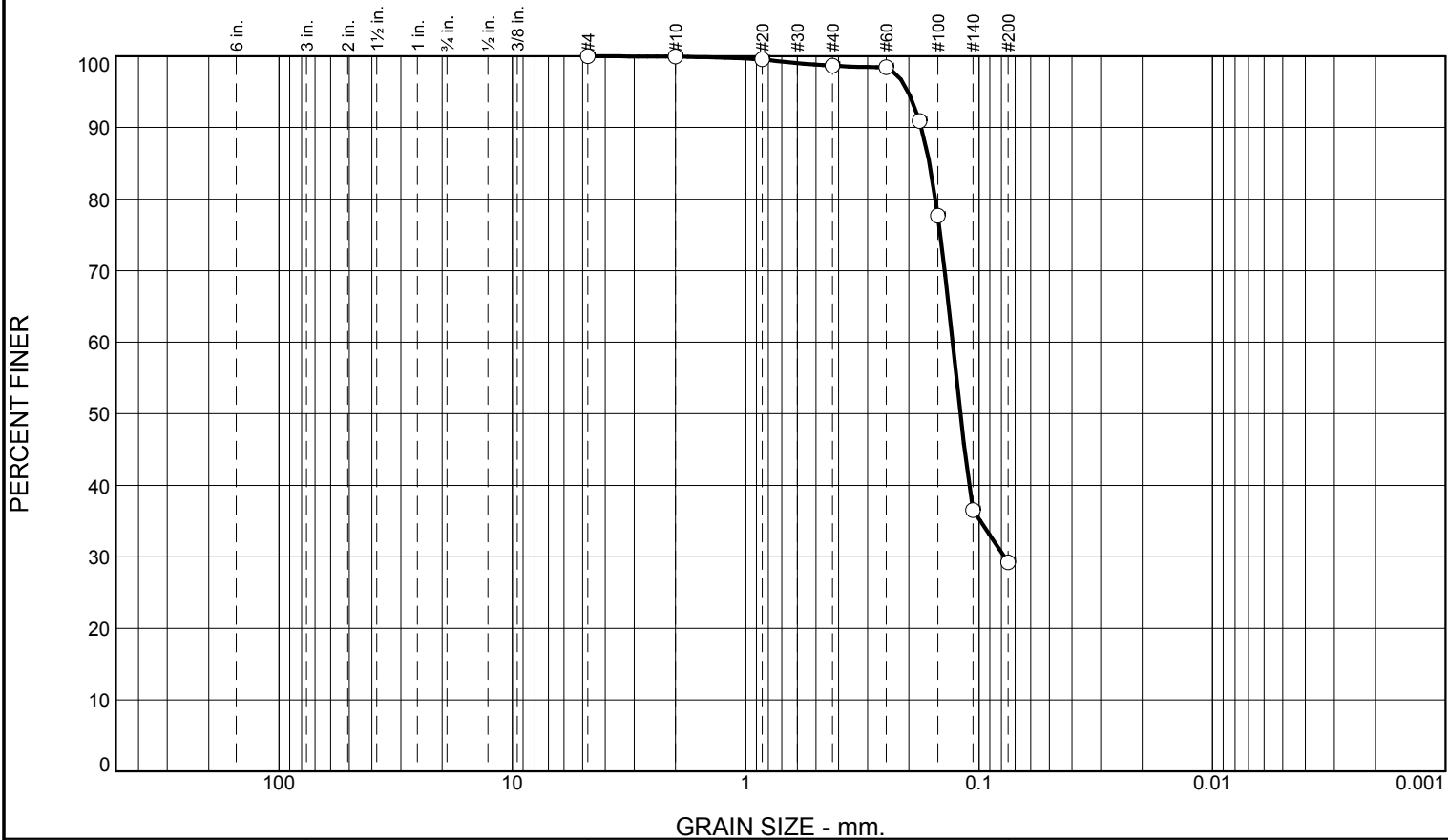
Client: ETM (England-Thims & Miller Inc)
Project: JEA Galvanized Pipe

Project No: 30388

Figure

Tested By: SB Checked By: SB

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	1.3	69.5	29.2	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#4	100.0		
#10	100.0		
#20	99.6		
#40	98.7		
#60	98.5		
#80	90.9		
#100	77.7		
#140	36.5		
#200	29.2		

* (no specification provided)

Material Description		
Gray Brown Clayey Fine Sand		
<div> <div> Atterberg Limits </div> <div> PL= <div> LL= PI= </div> </div> </div>		
<div> <div> Coefficients </div> <div> D₉₀= 0.1767 D₅₀= 0.1202 D₁₀= D₈₅= 0.1630 D₃₀= 0.0779 C_u= D₆₀= 0.1298 D₁₅= C_c= </div> </div>		
<div> <div> Classification </div> <div> USCS= AASHTO= A-2-6 </div> </div>		
<div> Remarks </div>		

Source of Sample: B41 Depth: 4.50-7.00
 Sample Number: 3

Date:



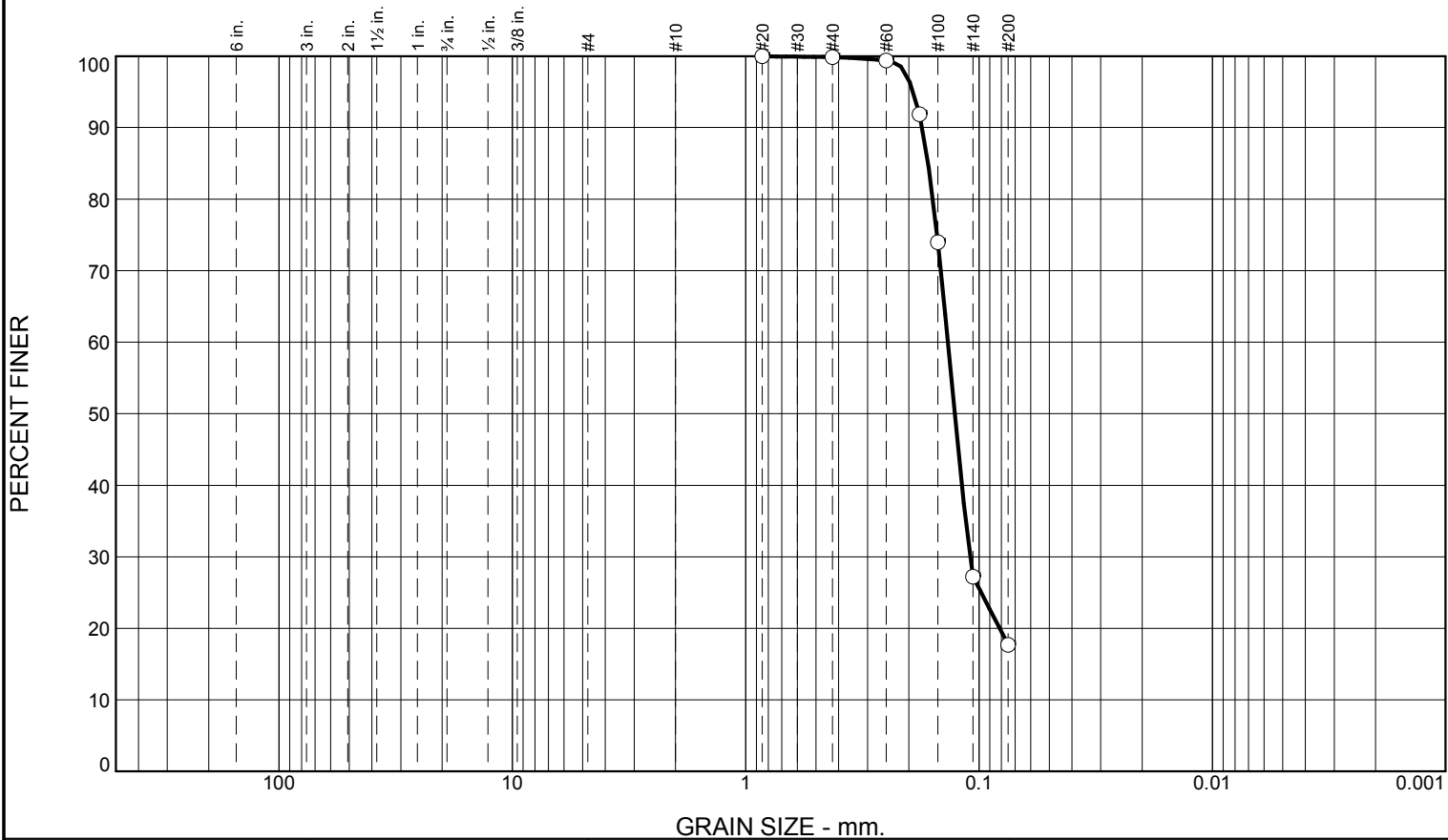
Client: ETM (England-Thims & Miller Inc)
 Project: JEA Galvanized Pipe

Project No: 30388

Figure

Tested By: SB Checked By: SB

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.0	0.0	0.1	82.2	17.7	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
#20	100.0		
#40	99.9		
#60	99.4		
#80	91.9		
#100	74.0		
#140	27.2		
#200	17.7		

Material Description
Gray and Dark Gray Clayey Fine Sand

Atterberg Limits
 PL= LL= PI=

Coefficients
 D₉₀= 0.1752 D₈₅= 0.1653 D₆₀= 0.1358
 D₅₀= 0.1270 D₃₀= 0.1091 D₁₅=
 D₁₀= C_u= C_c=

Classification
 USCS= AASHTO= A-2-6

Remarks

* (no specification provided)

Source of Sample: B48
Sample Number: 3

Depth: 8.00-10.00

Date:



ECS FLORIDA, LLC
7064 Davis Creek Road
Jacksonville, Florida 32256
Phone: (904) 880-0960
Fax: (904) 880-0970

Client: ETM (England-Thims & Miller Inc)
Project: JEA Galvanized Pipe

Project No: 30388

Figure

Tested By: SB Checked By: SB

LABORATORY TEST PROCEDURES

Percent Fines Content

The percent fines or material passing the No. 200 mesh sieve of the sample tested was determined in general accordance with the latest revision of ASTM D 1140. The percent fines are the soil particles in the silt and clay size range.

Natural Moisture Content

The water content of the sample tests was determined in general accordance with the latest revision of ASTM D 2216. The water content is defined as the ratio of “pore” or “free” water in a given mass of material to the mass of solid material particles.